## Instruction Manual <br> Model 640 <br> Electrometer

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## AS A MICROVOLTMETER:

RANGE: 30 microvolts full scale to 30 volts in thirteen $1 x$ and $3 x$ ranges.
ACCURACY: $+1 \%$ of full scale on 30 -volt to 300 -microvolt ranges, decreasing to $+5 \%$ on 30 -microvolt range.
2ERO DRIFT: Less than $35 \mu \mathrm{~V}$ in the first hour and in each succeeding 24 -hour period after 1 -hour warm-up. Less than $35 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$.
METER NOISE: Less than 0.4 microvolt rms ( 2 microvolts $\mathrm{p}-\mathrm{p}$ ) with 1 megohm or less input resistance on most sensitive range.
INPUT IMPEDANCE: Greater than $10^{16}$ ohms shunted by less than 2 picofarads. Input resistance may also be selected in four steps from $10^{6}$ to $10^{12}$ ohms.
RISE TTME ( $10 \%-90 \%$, with up to 100 megohms source resistance and no external capacitance): Less than 10 milliseconds on 1 -mv and higher ranges, increasing to 6 seconds on the $30-\mu \mathrm{V}$ range.

## AS AN AMMETER:

RANGE: $10^{-15}$ ampere full acale to $3 \times 10^{-5}$ ampere in twenty-two $1 x$ and $3 x$ ranges using built-in highmegohm resistors and range switch.
ACCURACY: $\pm 3 \%$ of full scale on $3 \times 10^{-5}$ to $10^{-11}$ ampere ranges using the smallest recommended multiplier setting; $+4 \%$ of full scale on $3 \times 10^{-12}$ to 10-15 ampere ranges. Instrument can be calibrated to $\pm 2 \%$ accuracy below $10^{-9}$ ampere with external voltage supply and built-in calibrating circuits.
METER NOISE: Less than $2 \times 10^{-17}$ ampere rms ( $10^{-16}$ ampere $p^{-p}$ ) on $10^{-15}$ ampere range when overdamped on $10^{-16}$ ampere tms ( $5 \times 10^{-16}$ ampere $p-p$ ) when critically damped, Less than 24 alpha pulses per hour as observed on the 30 -millivolt range.
DAMPING: Variable from critical damping to overdamping with 20 picofarads shunting the high-megohm resistor.
CURRENT STABILITY: Better than $5 \times 10^{-17}$ ampere/day after stabilization. Long-term drift is non-cumulative.
MAX. EXTERNAL CAPACITANCE (Feedback current ranges): 500 pf .
RISE TIME: Seconds, from $10 \%$ to $90 \%$.

| Recommended <br> Full-Scale <br> Ranges | Resistor <br> Value, <br> ohms | Critically <br> Damped; <br> no external <br> capacitance | Overdamped; <br> up to <br> maximum <br> capacitance |
| :---: | :---: | :---: | :---: |
| $10^{-15}$ to $3 \times 10^{-11}$ | $10^{12}$ | 1.5 | 44 |
| $10^{-12}$ to $3 \times 10^{-9}$ | $10^{-10}$ | 0.2 | 0.5 |
| $10^{-11}$ to $3 \times 10^{-7}$ | $10^{8}$ | 0.05 | 0.05 |
| $10^{-9}$ to $3 \times 10^{-5}$ | $10^{-9}$ | 0.01 | 0.01 |

## AS A COULOMBMETER/CURRENT INTEGRATOR:

RANGE (recomended): $2 \times 10^{-14}$ coulombs full scale to $6 \times 10^{-10}$ coulombs in ten $2 x$ and $6 x$ ranges.

ACCURACY: Integrating capacitance is 20 picofarads $\pm 0.25 \%$.
METER NOISE: Less than $3 \times 10^{-16}$ coulomb rms ( $1.5 \times$ $10^{-15}$ coulomb $\mathrm{p}-\mathrm{p}$ ) on lowest recommended range. Less than 24 alpha pulses per hour as observed on 30 -millivolt range.

## AS AN AMPLIFIER:

RECORDER OUTPUT: $\pm 1$ volt at up to 1 ma for fullscale input. Output polarity is opposite input polarity.
Gain: 0.033 to $3.3 \times 10^{4}$.
Frequency Response (Within 3db): dc to 0.07 cps at a gain of $3.3 \times 10^{4}$, rising to 35 cps at a gain of $10^{3}$ or below.
Noise: Below 1 cps : same as meter noise for specified function. Above 1 cps : less than $2 \%$ of full output $p-p$ on the $30-v$ to $10-\mathrm{mv}$ ranges, increasing to $10 \%$ on the 1 mv and lower ranges.
UNITY GAIN OUTPUT: At dc, output is equal to input within $.01 \%$ or $10 \mu \mathrm{~V}$, exclusive of zero drift, for output currents of $100 \mu \mathrm{a}$ or less.

## GENERAL:

ZERO CHECK: Remote "zero" solenoid shorts input to low through 1 kilohm in volts position, to feedback in current or integrate position.
ISOLATION: Circuit ground to chassis ground: Greater than $10^{9} \Omega$ shunted by $0.05 \mu \mathrm{f}$. Circuit ground may be floated up to $\pm 100 \mathrm{~V}$ with respect to main case. Head case is circuit ground. On battery operation, instrument may be completely isolated from power line and ground.
POLARITY: Meter switch selects left-zero (positive or negative) or center-zero scales. Meter switch does not reverse polarity of output.
CONNECTORS: Input: Special type, mates with many comercially available ion chambers and other accessories (adapter to UHF included). Low: Binding post. Recorder output: Amphenol 80-PC2F. UnityGain Output and Case Ground: Binding posts.
POWER:
Line Operation: 105-125 or 210-250 volts (switch selected), 50 or $60 \mathrm{cps}, 20$ watts.
Battery Operation: Rechargeable nickel-cadmium 6volt battery pack, 8 hours full charge to complete discharge. For maximum battery life, battery operation recommended for no more than 6 consecutive hours before recharge.
DIMENSIONS, WEIGHT:
Power Chassis: $7^{\prime \prime}$ high $\times 8-3 / 4^{\prime \prime}$ wide $\times 10^{\prime \prime}$ deep; net weight, 14 lbs.
Amplifier Head: $6^{\prime \prime}$ high x $5^{\prime \prime}$ wide $\times 6^{\prime \prime}$ deep; net weight, 6 lbs.
ACCESSORIES SUPPLIED: Connecting Cable: 5 ' long, connects head to main chassis. UHF Adapter: adapts input to UHF connector. Shield Cap. Mating output connector. Internally mounted nickel-cadmium battery pack and charging circuit.

## SECTION 1. GENERAL DESCRIPTION

l-1. GENERAL. The Model 640 Vibrating Capacitor Electrometer is an ultra-stable, solid-state microvolt electrometer.
a. As a Microvoltmeter. When used as a microvoltmeter, the Model 640 has an input resistance greater than $10^{16}$ ohms with thirteen ranges from 30 microvolts full scale to 30 volts.
b. As a Picoammeter. When used with the built-in, high-megohm SHUNT RESISTORS, the instrument has twenty two ranges from $10^{-15}$ ampere full scale to $3 \times 10^{-5}$ ampere.
c. As a Coulombmeter. By switching an accurate guarded capacitor in the feedback loop the instrument is useful as a coulombmeter or current integrating amplifier. In the CURRENT INTEGRATE mode the instrument has ten ranges from $2 \times 10^{-14}$ coulomb full scale to $6 \times 10^{-10}$ coulomb.
d. As an Amplifier. The analog OUTPUT permits use of the instrument as a very stable, variable gain amplifier.

## 1-2. FEATURES.

a. Excellent Stability. A stability specified at better than $5 \times 10^{-17}$ ampere/day is useful for mass spectrometer, resistivity, and ion chamber measurements.
b. Remote Input Head. A compact Remote Input preamplifier permits convenient set up of an experiment.
c. High Input Impedance. Guarding plus the use of sapphire insulation provides an input resistance greater than $10^{16}$ ohms shunted by less than 2 picofarads.
d. Battery or Line Operation. A choice of battery or line operation permits complete isolation (in battery mode) from power line when required.
e. Built-In Shunt'Resistors. Four high-megohm shunt resistors can be switch selected (Input Head) for shunt or feedback current measurements.

table 1-1.
Front Panel Controls.

| Control | Functional Description | Paragraph |
| :---: | :---: | :---: |
| POWER Switch (S301) | Controls the power to the instrument. | 2-3, a |
| FUNCTION Switch (S402) | Selects the mode of operation. | 2-3, b |
| RANGE Switch (S403) | Selects the meter sensitivity. | 2-3, c |
| METER Switch (S404) | Selects meter polarity, center scale, and meter off. | 2-3, d |
| 2ERO Controls |  |  |
| MEDIUM (S407) | Adjusts meter zero. | 2-3, e |
| FINE (R431) | Adjusts meter zero (fine control). | 2-3, e |
| ZERO CHECK Switch (S401) | Permits a meter zero check. | 2-3, f |

TABLE 1-2.
Input Head Controls and Terminals.

| Control | Functional Description | Paragraph |
| :---: | :---: | :---: |
| SHUNT RESISTOR Switch (S102) | Selects a shunt or feedback resistor from $10^{6}$ to $10^{12}$ ohms. | 2-2, a |
| ZERO CHECK Switch (S101) | Permits a meter zero check. | 2-2, b |
| FEEDBACK Terminal (J103) | Useful for unity gain or guarded measurements. | 2-2, d |
| Input Receptacle (J105) | Provides connection to Input High | 2-2, c |
| DAMPING Control (R108) | Adjusts damping for CURRENT INTEGRATE function. | 2-2, e |



FIGURE 2. Front Panel Controls.


FIGURE 3. Input Head Controls.

TABLE 1-3.
Rear Panel Controls and Terminals.

| Control | Functional Description | Paragraph |
| :---: | :---: | :---: |
| REMOTE HEAD Receptacle (J405) | Provides connection to Input Head. | 2-4, a |
| OUTPUT Receptacle (3404) | Provides an analog output. | 2-4, b |
| GND Terminal (J406) | Connection to Main Chassis ground. | 2-4, c |
| LO Terminal (J402) | Provides connection to Input LO. | 2-4, d |
| FEEDBACK Terminal (J403) | Useful for unity gain or guarded measurements. | 2-4, e |
| COARSE ZERO Switch (S405) | Adjusts meter zero (coarse control). | 2-4, f |
| LINE VOLTAGE Switch (S302) | Sets instrument for either 117 or 234 V power. | 2-4, g |
| Line Power Fuse (F301) | Protects line power circuit. | 2-4, h |
| Battery Power Fuse (F302) | Protects battery power circuit. | 2-4, i |
| 1V-1MA Switch (S406) | Sets OUTPUT for either IV or 1MA. | 2-4, j |
| IMA CAL Control (R423) | Adjusts OUTPUT current for .95-1.05 MA. | 2-4, k |



FIGURE 4. Rear Panel Controls and Terminals.

## SECTION 2. OPERATION

## 2-1. INPUT CONSIDERATIONS.

a. Input Head Connections.

1. Remote Cable. A shielded coaxial cable (5 feet long) is supplied to permit remote location of the Input head from the Main Chassis. An accessory Model 6401 Cable ( 25 feet long) also can be used without degradation of specifications.
2. Mounting. The Input Head Chassis can be custom mounted as described in paragraph 2-12.
3. Input Assembly. This assembly (J105) consists of an insulated input High terminal (center post) and a machined housing which is input Low. High input resistance (over $10^{16}$ ohms shunted by less than 2 picofarads) is maintained by use of sapphire insulation.
a.) Custom Connections. The input housing has been designed to easily adapt for use with ion chambers and other applications where high input impedance and low capacitance is required. Dimensions of the input housing are given in Figure 5.
b.) UHF Adapter. The adapter supplied with the Model 640 is useful when quick connections must be made using standard UHF cables. However, this adapter is limited to measurements above $10^{-13}$ ampere or source resistances below $10^{14}$ ohms.
c.) GR874 (General Radio) Adapter. This accessory adapter is available for use with GR874 Series coaxial accessories. The limitations of this adapter are similar to those for the UHF adapter.
b. Insulation, Use high resistance, low-loss materials such as sapphire, teflon, polyethylene or polystyrene for insulation of the input circuit.


FIGURE 5. Dimensions of Input Housing.

## NOTE

The input terminal and sapphire insulator should be protected from contamination so that the insulation will not be degraded. Clean, dry connections and cables are very important to maintain the value of all insulation materials. Even the best insulation can be compromised by dust, dirt, solder, flux, films of oll or water vapor. A good cleaning agent is methyl alcohol, which dissolves most common dirt without chemically attacking the insulation.
c. Noise Consideration. The limit of resolution in voltage and current measurements is determined largely by the noise generated in the source. Stray low-level noise is present in some form in nearly all electrical circuits. The instrument does not distinguish between stray and signal voltages since it measures the net voltage. When using the microvolt ranges consider the presence of low-level electrical phenomena such as thermocouples (thermoelectric effect), flexing of coaxial cables (trioelectric effect), apparent residual charges on capacitors (die-lectric absorption), and battery action of two terminals (galvanic action).

1. Thermal EMFS. Thermoelectric potentials (thermal emfs) are generated by thermal gradients between two functions of dissimilar metals. These can often be large compared to the signal to be measured. To minimize the drift caused by thermal emfs, use pure copper leads wherever possible in the source circuit. Drift can also be minimized by maintaining constant junction temperatures especially by using a large heat sink near the connections. The Keithley accessory Model 1483 Low Thermal Connection Kit contains all necessary materials for making very low thermal copper crimp connections for minimizing thermal effects.
2. AC Electric Fields. The presence of electric fields generated by power lines or other sources can have an effect on instrument operation. AC voltages which are very large with respect to the full-scale range sensitivity could drive the ac amplifier into saturation, thus producing an erroneous de output. Proper shielding as described in paragraph 2-1, d can minimize noise pick-up when the instrument is in the presence of large ac fields or when very sensitive measurements are being made.
3. Magnetic Fields. The presence of strong magnetic fields can be a potential source of ac noise. Magnetic flux lines which cut a conductor can produce large ac noise especially at power line frequencies. The voltage induced due to magnetic flux is proportional to the area enclosed by the circuit as well as the rate of change of magnetic flux. For
example, the motion of a 3 -inch diameter loop in the earth's magnetic field will induce a signal of several tenths of a microvolt. One way to minimize magnetic pickup is to arrange all wiring so that the loop area enclosed is as small as possible (such as twisting input leads). A second way to minimize magnetic pickup is to use shielding as described in paragraph 2-1, d.

## d. Shielding.

1. Electric Fields. Shielding is usually necessary when the instrument is in the presence of very large ac fields or when very sensitive measurements are being made. The shields of the measurement circuit and leads should be connected together to ground at only one point. This provides a "tree" configuration, which minimizes ground loops.
2. Magnetic Fields. Magnetic shielding is useful where very large magnetic fields are present. Shielding, which is available in the form of plates, foil or cables, can be used to shield the measuring circuit, the lead wires, or the instrument itself.
e. Moisture. The Model 640 Input Head is shipped with a dessicant bag sealed inside. This bag soaks up the moisture inside the Input Head to insure optimum operation. The dessicant bag, however, will eventually become saturated. At this point the Model 640 offset will increase beyond the specified amount. When this happens take off the bottom cover of the Input Head to remove the dessicant bag. Reactivate it according to the instructions on the bag.
f. Guarding. Use of a "driven guard" or "guard ring" is important when making peasurements from source resistances greater than $10^{12}$ ohms. The guard minimizes the effects of leakage currents from input High to input Low.

2-2. INPUI HEAD CONTROLS AND TERMINALS. The Input Head is show in Figures 1 and 3. The operation of each control or terminal is described as follows:
a. SHUNT RESISTOR Switch (S102). This switch selects 5 positions corresponding to the shunt resistor (across input of feedback) required by the measurement. The switch positions are $10^{6}, 10^{8}, 10^{10}, 10^{12}$ and "OPEN". The "OPEN" position has no resistor connected.
b. ZERO CHECK Switch (S101). This switch is a normally-open contact type switch permitting a check of meter zero. (The ZERO CHECK Switch (S401) on the Main Chassis has the same function). The ZERO CHECK switch shunts the input HI to LO (in VOLTAGE function) by 1000 ohms.
c. Input Receptacle (J105). This receptacle provides input connection to the Mode 1640 Input High and Input Low.
d. FEEDBACK Terminal (J103). This terminal is used for unity gain or guarded measurements.
e. DAMPING Control (R108). (Not Shown). This control permits adjustment of the damping for CURRENT INTEGRATE operation. When the control is set fully clockwise to "MAX" damping, the rise time is approximately 44 seconds with a $10^{12}$ shunt resistor. When the control is set fully counter-clockwise to "MIN" damping, the rise time corresponds to the critically damped or CURRENT FAST condition as given in the specifications.

2-3. FRONT PANEL CONTROLS. The front panel controls are shown in Figures 1 and 2. The operation of each control is described as follows:
a. POWER Switch (S301). This switch has four positions designated AC, OFF, BATTERY, and BATT TEST.

1. AC Position. This position permits normal operation of the instrument when the power cord is connected to line power. (The battery charging circuit operates in this position.)
2. OFF Position. This position disables both AC and BATTERY power to the electrometer circuits except for the battery charging circuit which operates in this position.
3. BATYERY Position. This position permits normal operation of the instrument when the internal battery pack is satisfactorily charged.
4. BATT TEST Position. This position permits a check of the battery voltage as indicated by the meter.
b. FUNCTION Swtich (S402). This switch has three positions designated VOLTAGE, CURRENT FAST, and CURRENT INTEGRATE.
5. VOLTAGE Position. This position connects the electrometer as a very sensitive, high impedance voltmeter with the SHUNT RESISTORS connected in shunt across the input.
6. CURRENT FAST. This position connects the electrometer as a feedback picoammeter which neutralizes the effect of input capacitance and increase response speed. The SHUNT RESISTORS are connected in the feedback loop of the amplifier.
7. CURRENT INTEGRATE. This position connects the 20 picofarad guarded capacitor in the feedback loop of the amplifier.
c. RANGE Switch (S403). This switch has thirteen positions corresponding to full scale voltage sensitivity from 30 microvolts to 30 volts.
d. METER Switch (S404). This switch has 4 positions designated OFF, + , - , and CENTER ZERO.
8. OFF Position. This position disables the meter movement to protect against overloads. This position has no effect on the OUTPUT voltage when using a recorder or other instrument.
9. "f" and " - " Positions. These positions select the polarity of the meter only. The OUTPUT voltage is not affected by these positions.
10. CENTER ZERO. This position sets the meter circuit so that zero is indicated at center scale (mid-scale), The deflection of the meter corresponds to one-half RANGE setting. The OUTPUT voltage is not affected by this position.
e. ZERO Switch. This switch is a dual-concentric control.
11. MEDIUM Control (S407). This control is the outer knob with eleven positions which adjust the meter-zero.
12. FINE Control (R431). This control is the inner knob which permits fine meter-zero adjustment.
E. ZERO CHECK (S401). This switch is a normallyopen contact-type switch permitting meter-zero check. The ZERO CHECK switch shunts the input HI to input LO (in voltage function) by 1000 ohms.

2-4. REAR PANEL CONTROLS AND TERMINALS. The rear panel controls and terminals are shown in Figure 4. The operation of each control or terminal is described as follows.
a. REMOTE HEAD Receptacle (J405). This receptacle is a 24-pin connector (Ampheno1 57-40240) which mates with the interconnecting cable between the Main Chasis and Input Head (Remote Head). Two mechanical retaining clips are provided on the receptacle to secure the mating plug (P405).
b. OUTPUT Receptacle (J404). This connector provides an analog output for recording or monitoring purposes. The output is -1 volt at up to 1 mA for full scale input. The output polarity is opposite the input polarity. The front panel METER switch has no effect on the polarity of the analog output.
c. GND Terminal (J406). This terminal is connected to Main Chassis ground and the outside shell of connector J405. With no connection between GND and LO (shorting link removed), the INPUT LO to Main Chassis ground isolation is greater than $10^{9}$ shunted by .05 microfarad.
d. LO Terminal (J402). This terminal is connected to INPUT LO on INPUT HEAD.
e. FEEDBACK Terminal (J403). This terminal is used for unity gain or guarded measurements. The teminal (J403) on the Main Chassis is connected to $J 103$ on the INPUT HEAD by way of the remote cable.
f. COARSE ZERO Switch (S405). This switch has ten positions for adjusting the meter-zero circuit. This switch should only be used when the FINE and MEDIUM

2ERO Controls do not provide sufficient range of control.
g. LINE VOLTAGE Switch (S302). This switch sets the instrument for either 117 or 234 volt rms linepower. The line-power fuse (F301) should be checked for proper line voltage rating.
h. Line Power Fuse (F301). This fuse protects the power supply circuits when $117-234 \mathrm{~V}$ line power is used.

| Line Voltage | Fuse Rating |
| :---: | :--- |
| 117 V | $1 / 4 \mathrm{amp}, 3 \mathrm{AG}$ |
| 234 V | $1 / 8 \mathrm{amp}$, 3AG |

1. Battery Power Fuse (F302). This fuse protects the power supply circuits when battery power is used. Fuse rating: $3 / 4 \mathrm{amp}$, 3 AG .
2. 1V-1MA Switch (S406). This switch sets the oUTPUT for either 1 volt or 1 mA .
k. lMA CAL Control (R423). This control permits adjustment of the OUTPUT (with IV-1MA Switch set to 1 MA ) over the range 0.95 to 1.05 mA .

## 2-5. OPERATING CONSIDERATIONS.

## a. Mode of Operation.

1. AC Line-Power. The Model 640 can be operated using ac line- power at 117 V or $234 \mathrm{~V}, 50$ or 60 Hz . To operate, set LINE VOLTAGE Switch (S302) to 117 or 234, check for proper rated fuse (F301), and connect the line cord. Set the POWER Switch (S301) to " $A C$ " operation.
2. Battery Power. The Model 640 can be operated using battery power supplied by a rechargeable 6 volt nickel~cadmium battery pack.
a.) To check the battery charge, set the POWER Switch to "BATT TEST" position. The meter should indicate $+6 V$ or greater if charge is satisfactory.
b.) To recharge the battery pack, connect the power cord to ac power. Set the POWER Switch to "OFF". (The battery will automatically recharge when the POWER Switch is in either "AC" or "OFF" positions). Battery charging-time is approximately 16 hours for full charge after 8 hours of continuous use.
3. AC to Battery Switching. The Model 640 can be modified so that it will automatically switch from "AC" operation to "BATTERY" operation if the line power fails. An explanation of this modification is given in paragraph 3-4 in the Circuit Des $\rightarrow$ cription section.
b. Warm-up. If the instrument is to be used for very sensitive measurements, allow the instrument to stabilize for an hour or more. The POWER Switch can be set at either "AC" or "BATTERY".
c. Meter Zero. The meter zero circuit utilizes three controls FINE, MEDIUM, and COARSE.
4. After warm-up, set the METER Switch to CENTER ZERO.
5. Adjust the MEDIUM 2ERO Control for centerzero meter position. (The rear panel COARSE ZERO Switch can be used if meter reads off scale).
6. Increase sensitivity using the RANGE Switch and adjust the FINE ZERO Control for center-zero meter indication.

2-6. VOLTAGE FUNCTION.
a. General. When the FUNCTION Switch is set to the VOLTAGE position, the Model 640 operates as a high in-put-impedance electrometer.
b. Input Impedance. The input resistance (HI to LO) is greater than $10^{16}$ ohms shunted by less than 2 picofarads. This specification is valid only for the SHUNT RESISTOR Switch set to "OPEN" with no degradation of the input $H I$ to input $L O$ insulation. The input resistance can be lowered by selecting, SHUNT RESISTOR values in four steps from $10^{6}$ to $10^{12}$ ohms.

## c. Microvoltmeter Measurements.

1. Theory, The electrometer, when used as a microvoltmeter, can be illustrated as shown in Figure 6. In this configuration the instrument is useful for making sensitive measurements from 30 microvolts full scale to 30 volts. The sensitivity is adjusted by the RANGE Switch (S403) represented by $\mathrm{R}_{\mathrm{A}}$. The input voltage is represented by $e_{i}$. The voltage $e_{A}$ is defined by the following expression,

$$
e_{A}=e_{1}\left(\frac{K}{K}+T\right)
$$

where $K$ is the amplifier loop gain.
Therefore $i_{A}=\frac{e_{A}}{R_{A}} \geq \frac{e_{i}}{R_{A}}$ where $R_{A}$ is selected by the RANGE Switch (S403).
2. Voltage Measurement.
a.) High Impedance, Although the electrometer has a very high input impedance, the useability of the Model 640 as a microvoltmeter is limited by the thermal (Johnson) noise generated in the source impedance. Refer to paragraph 2-10 for a complete discussion of thermal notse.
b.) Low Impedance. The Mode 1640 can be used on the more sensitive ranges by setting the SHUNT RESISTOR Switch to $10^{12}$ ohms or lower. The loading effects should be considered when measuring high source-impedance.
3. Current Measurement. The Model 640 can be used for current measurements since the microvoltmeter measures the voltage across a known shunt resistor selected for $10^{6}, 10^{8}, 10^{10}$, or $10^{12}$ ohms. Current can be calculated by the ratio of voltage reading to shunt resistance. Use this technique where low noise is important, although faster response is provided by setting the FUNCTION Switch to CURRENT FAST as described in paragraph 2-7.
4. Unity Gain Measurements. The Model 640 can be used for measuring a potential from a very high impedance source with . 025\% accuracy. Connect a digital voltmeter (or differential) to FEEDBACK and LO terminals as shown in Figure 7.


FIGURE 6. Voltage Function With Shunt Resistor $\mathrm{R}_{\mathrm{S}}$


FIGURE 7. Use of FEEDBACK Connection.


FIGURE 9. Guarded Measurement.

## 2-7. CURRENT FAST FUNCTION.

a. General. When the FUNCTION Switch is set to the CURRENT FAST position, the Model 640 operates as a feedback ammeter with feedback resistors selected by the SHUNT RESISTOR Switch in four steps from $10^{6}$ to $10^{12}$ ohms.

## b. Feedback Ammeter Measurements.

1. Theory. The Model 640, when used as a feedback ammeter, can be illustrated as shown in Figure 8. In this configuration the instrument is useful for making sensitive measurements from $10^{-15}$ ampere full. scale. Response speed is greatly improved compared to the VOLTAGE FUNCTION configuration since the effect of input capacitance is largely neutralized.

TABLE 2-1.
Input Resistance in CURRENT FAST Function.

| RANGE | Current | Input <br> Resistance | Input <br> Voltage |
| :--- | :--- | :---: | :--- |
| 10 V | $1 \times 10^{-11}$ | $10^{8}$ | 1 mV |
| 1 V | $1 \times 10^{-12}$ | $10^{8}$ | $100_{\mu \mathrm{V}}$ |
| 100 mV | $1 \times 10^{-13}$ | $10^{8}$ | $10_{\mu} \mathrm{V}$ |
| 10 mV | $1 \times 10^{-14}$ | $10^{8}$ | $l_{\mu \mathrm{V}}$ |
| 1 mV | $1 \times 10^{-15}$ | $10^{8}$ | $0.1_{\mu \mathrm{V}}$ |
|  |  |  |  | The input voltage drop and effective ammeter input resistance is given for each RANGE setting as in Table 2-1.



FIGURE 8. Current Fast Function.

## 2. Current Measurement.

a.) Rise Time. The actual rise time for a particular measurement depends on the shunt resistor and residual capacitance across the feedback loop. The specified rise time ( 10 to $90 \%$ ) is given in the specifications for each resistor value. These rise times are for a critically damped condition where no external capacitance is present, Additional external capacitance can be connected between the FEEDBACK terminal and input HI
b.) Guarded Measurements. The Model 640 can be used for guarded resistance measurements using the FEEDBACK Terminal and Input HI connections as shown in Figure 9 . Since $\overline{E_{B}}$ and $R_{B}$ develop a known current $I_{B}$, then the electrometer will indicate the voltage developed across $R x$ (unknown resistance).

$$
\mathrm{Rx}=\frac{\mathrm{E}_{0}}{\mathrm{I}_{\mathrm{B}}}=\frac{\mathrm{E}_{0}}{\mathrm{E}_{\mathrm{B}}} \times \mathrm{R}_{\mathrm{B}}
$$

## 2-8. CIJRRENT INTEGRATE FUNCTION.

a. General. When the FUNCTION Switch is set to the CURRENT INTEGRATE position the Model 640 operates as a feedback ammeter with damping.

## b. Feedback Ammeter Measurements.

1. Theory. The Mode1 640 operation can be illustrated as shown in Figure 10. In this configuration the DAMPING Control is set to 'MAX" position so that a 20 pf capacitance is connected in the feedback loop (SHUNT RESISTOR Switch set to "OPEN"). The current measured is determined by the following equation,

$$
I=C \int_{t_{0}}^{t_{f}} \frac{d E}{d T}=C\left(\frac{\Delta E}{\Delta t}\right)=\frac{d Q}{d T}
$$

where $I=$ current in amperes.
$\mathrm{C}=$ feedback capacitance $\left(2 \times 10^{-11}\right)$.
$\Delta E=$ change in the meter reading during time interval At.
$\Delta t=$ time interval of measurement.
2. Variable Damping. When the DAMPING Control (R108) is adjusted. counter-clockwise, the Model 640 can be used for current measurements with variable damping.

## 2-9. SHUNT RESISTOR CALIBRATION.

a. General. The Model 640 can be calibrated for use as an ameter accurate to $\pm 0.25 \%$.
$\mathrm{b}_{\mathrm{f}}$. Theory. Calibration of the high value ( $10^{10}$, $10^{12}$ ) shunt resistors can be accomplished using a current integrating technique. An accurately known voltage source can be connected in series with the shunt resistor forming a current source where $I=$ V/R. With FUNCTION Switch set to CURRENT INTEGRATE the meter reading $E M$ is a function of capacitance $C$ and the integral of the current.

$$
\begin{aligned}
E_{M} & =\frac{1}{C} \int \text { idt } \quad \text { or } \\
\Delta E_{M} & =\frac{1}{C} \Delta T=\left(\frac{V}{R C}\right) \Delta T
\end{aligned}
$$

Solving for $R$,

$$
R=\frac{V}{C}\left(\frac{T-T O}{E-E O}\right)
$$

Where $\quad R=$ shunt resistance, ohms.
$V=$ source voltage.
$C=$ integrating capacitor (20 pf).
$E-E O=$ change in voltage indication.
$T-T o=t i m e$ interval for voltage change.
Since the accuracy of $C$ is $\pm .25 \%$ the overall accuracy of the calibration will depend on the accuractes of the voltage source $V$, the meter accuracy $E_{M}$, and the time accuracy $T$. (To obtain the best possible accuracy, measure the analog OUTPUT using a $0.01 \%$ digital voltmeter.) Refer to Figure 11 for circuit connections.

## c. Calibration Procedure.

1. Set the FUNCTION Switch to CURRENT INTEGRATE.
2. Set the DAMPING to "MAX".
3. Apply the voltage source between P106 and input LO. (Remove the Input Head bottom cover for access).
4. Zero meter.
5. Select $10^{10}$ or $10^{12}$ SHUNT RESISTOR.
6. Measure time interval from zero to full scale on the meter. Record time interval T-To.
7. Calculate the value of $R$ using equation.


FIGURE 10. Equivalent Current Integrator.

FIGURE 11. Current Integrate - Shunt Resistor Calibration.

2-10. ANALOG OUTPUTS.
a. OUTPUT Terminal (J404). This terminal provides an analog output for recording or monitoring purposes.

1. IV Output. With the IV-1MA Switch (S406) set to "lV" the output is +1 volt corresponding to a full scale input. The polarity of the output is opposite the input signal.

$$
\text { Gain: } 0.033 \text { to } 3.3 \times 10^{4}
$$

Frequency Response (Within 3 db ): dc to 0.07 cps at a gain of $3.3 \times 10^{4}$, rising to 35 cps at a gain of $10^{3}$ or below.

Noise: Below lcps: same as meter noise for specified function. Above 1 cps : less than $2 \%$ of full output $\mathrm{p}-\mathrm{p}$ on the $30-\mathrm{v}$ to $10-\mathrm{mv}$ ranges, increasing to $10 \%$ on the 1 -mv and lower ranges.
2. LMA Output. With the IV-1MA Switch set to
"1MA" the output is approximately lMA for a full scale input.
b. Unity Gain Output. When the FUNCTION Switch is set to VOLTAGE the FEEDBACK terminal can be used for measuring a potential from a very high impedance source. At dc, the output is equal to the input within $.01 \%$ or $10 \mu \mathrm{~V}$, exclusive of zero drift, for output current of 100 pA or less.

## 2-11. THERMAL NOISE.

a. General. A common limitation of microvoltmeter measurements from high source impedances is the thermal noise (Johnson noise) generated in the source.
b. Theory. Thermal noise in an ideal resistance can be theoretically determined from the Johnson nolse equation as follows.

| $\mathrm{E}_{\mathrm{rms}}$ | $=\sqrt{4 \mathrm{~K} \cdot \mathrm{~T} \cdot \mathrm{R} \cdot \mathrm{F}}$ |
| ---: | :--- |
| Where |  |
| $\mathrm{E}_{\mathrm{rms}}$ | $=\quad$rms voltage noise generated in the <br> resistance. |
| T | $=$ temperature, oK. |
| R | $=$ ideal resistance, ohms. |
| F | $=$ amplifier bandwidth, Hz. |
| K | $=$ Boltzmann constant $\left(1.38 \times 10^{-10}\right.$ joules $\left./ \mathrm{o}_{\mathrm{K}}\right)$ |

The peak-to-peak noise is approximately five times the rms value (from experimental measurements), therefore the equation can be expressed as follows.

$$
\mathrm{Epp}=5 \times \mathrm{E}_{\mathrm{rms}}
$$

If the ambient temperature is $300^{\circ} \mathrm{K}$ (room ambient) then the peak-peak noise can be expressed as follows.

$$
\mathrm{Epp}=6.45 \times 10^{-10} \sqrt{\mathrm{RF}}
$$

c. Typical Example. The peak-peak thermal noise generated in an ideal source resistance can be illustrated as follows.

Given: Amplifier Bandwidth $\Delta \mathrm{F}=0.08 *$
$R=10^{12}$ ohms.
RANGE set to 1 MV .
Epp (typically) $=6.45 \times 10^{-10} \sqrt{10^{12} \times .08}$
Epp ~ $\quad 180$ uV Peak-Peak

$$
* \Delta F=\frac{1}{2 \pi R C}=\frac{1}{2 \pi 10^{12} \times 2 \times 10^{-12}} \approx .08
$$

## 2-12. MOUNTING DIMENSIONS.

a. Casting Dimensions. The overall dimensions of the Input Head Casting are shown in Figures 12 and 13.
b. Input Contact. The input contact is spring loaded with the dimensions from the base as shown in Figure 12.
c. Mounting the Base Plate. The Base Plate can be mounted on a machined surface for custom installation of the Input Head. The Base Plate is fastened to the Input Head casting using four type $6-32 \times 1 / 4$ screws. The rubber feet are attached to the base plate using type $6-32 \times 1 / 2$ Phillips Head screws and mating \# kep nuts. (The dessicant bag is also attached using this hardware). In order to mount the Input Head Casting to a surface plate, clearance holes must be drilled in the surface plate as shown in Figure 14. The Casting can be fastened to the surface using type 6-32 screws, The rubber feet should be removed and the four screws replaced. (Note that the holes drilled should provide sufficient clearance for the $6-32$ Phillips screw heads.)


## SECTION 3. CIRCUIT DESCRIPTION

3-1. GENERAL. The Model 640 is composed of an Input Head (Remote Preamplifier) and a Main Chassis (Amplifier and Power Supply).
a. High Impedance Microvoltmeter. When the FUNCTION Switch is set to VOLTAGE, the Model 640 operates as a very sensitive, stable voltmeter with very high input. impedance.
b. Vibrating Capacitor Electrometer. When the FUNCTION Switch is set to either CURRENT position, the Model 640 operates as a stable current and charge measuring instrument.

3-2. ELECTROMETER AMPLIFIER. The basic electrometer amplifier utilizes a vibrating-capacitor input preamplifier and variable-sensitivity amplifier. The overall amplifier operates as a very sensitive dc amplifier using a vibrating capacitor as an input signal modulator. The input signal is modulated, amplified and demodulated in the preamplifier circuit. The dc signal is filtered and amplified further by the main dc amplifier. Feedback is used extensively to provide gain accuracy and stability. A block diagram of the overall amplifier is shown in Figure 15.

3-3. INPUT HEAD. (Remote Preamplifier). The Input Head contains the input modulator, high-gain ac amplifier, oscillator and demodulator. The Shunt $\mathrm{Re}-$ sistors are connected across the overall amplifierfeedback using Switch sio2.
a. Vibrating Capacitor. A special capacitor is used consisting of two stationary plates and a vibrating membrane which is excited at a carrier frequency of approximately 400 kHz . The glass membrane has deposited metal surfaces and is sealed in an evacuated glass "bottle". This unique capacitor provides very high input-impedance and low drift. When driven at the carrier frequency (under proper conditions), the membrane resonates at approximately 6000 Hertz . Since the carrier (drive) frequency is much higher than the resonant frequency, the carrier frequency and harmonics does not appreciably affect the amplifier circuit.
b. Input Circuit. The input High signal is applied to receptacle Jl05 on the Input Head. The input LO is isolated from Main Chassis ground. A 10 megohm resistor (R105) prevents a rapid discharge of the vibrating capacitor back inco the source circuit. The modulated signal is applied to the first stage ac amplifier through a guarded, three-terminal air capacitor. (C105 which is $20 \mathrm{pF} \pm 0.25 \%$ ).
c. Zero Check Circuit. The ZERO CHECK control is a normally-open control which energizes solenoid Klol. When K 101 is energized, a contact connects input High to FEEDBACK through a 1000 ohm resistor. The input source and vibrating capacitor remain connected in the circuit during zero check. A loading error will result in the meter zero reading if the source resistance ( $\mathrm{R}_{\mathrm{S}}$ ) is less than 100 K in accordance with the following equation.

$$
\% \text { Error }=\frac{100}{R_{S}+1} \text {, where } \mathrm{R}_{\mathrm{S}} \text { is expressed in kilohms. }
$$



FIGURE 15. Block Diagram of Model 640.
d. AC Amplifier. The ac amplifier provides very high gain through the use of a two-stage amplifier and a phase splitter amplifier. An FET (Q101) provides a high input impedance. An emitter-follower stage (transistor Q102) provides impedance matching between Q101 and transistor Q106. Transistors Q103 Q104, Q105 and Q108 are switches providing gain adjustment to prevent oscillation on the higher ranges. Transistors Q107, Q109 and Q110 form a second stage ac amplifier. A phase splitter circuit is formed by transistors Q111 and Q112. A tuned circuit composed of integ. ckt. QALO1, inductor L101 and trimmer capacitor C124 provide attenuation of carrier frequency ( 6000 Hz ) second harmonic noise. The ac signal is synchronously demodulated by transistors Q506 and Q507 (located in the oscillator circuit).
e. Oscillator Circuit. The high frequency drive ( 400 kHz ) signal is generated by a tuned circuit consisting of transformer T501, capacitors C502, C503 and C504 and transistor Q501. Capacitor C502 adjusts the 400 kHz carrier frequency. Potentiometer R506 adjusts the gain of the drive circuit. The drive output is developed across transformer T502 and capacitor C509 to excite vibrating capacitor plates (pins 1 and 4). The actual signal is a modulated "envelope" as shown in Figure 28 in section 6. FET Q503 and integrated circuit QA501 form a wave-shaping circuit for phase and symmetry control. Integrated circuit QA502 is part of a phase control circuit for the demodulator output. Potentiometer $R 517$ adjusts the phase of the demodulator drive. Integrated circuit QA503 is part of a symmetry control circuit. Potentiometer R521 adjusts the demodulator on and off times (symmetry). Transistor Q505 controls the switching of demodulating transistors Q506 and Q507.

3-4. MAIN CHASSIS. The Main Chassis contains a dc amplifier circuit, meter circuit, sensitivity switching circuit, power supply circuit, and battery charging circuit as shown on Schematic 21383E.
a. DC Amplifier. A differential input stage is formed by FET's Q401 and Q402 and transistors Q403 and Q404. Potentiometer R404 provides de amplifier balance. Capacitors C401, C402, and C403 provide filtering of the demodulator ripple. FET Q405 and transistors Q406 and Q409 (Darlington amplifier) provide additional gain for driving the meter circuit and analog OUTPUT. Transistor $Q 408$ provides current limiting when the output is overloaded. Transistor Q407 provides a constant current for biasing purposes.
b. Meter Circuit. The meter circuit consists of a meter switch S404, a 1-MA meter movement (M401), and various meter circuit adjustments. The Meter switch has an OFF position (which shorts out the meter movement), "+" and "-" polarity positions (which connect the meter for either positive or negative deflection), and a ZERO CENTER position (which biases the meter such that center scale represents zero). Potentiometer R421 is an internal adjustment of the ZERO CENTER meter bias current. Potentiometer R455 is an internal adjustment of the meter calibration.
c. Zero Controls. Switch 5405 is a COARSE ZERO adjustment which can select up to 11 positions on a divider string (resistors R432 through R442). Switch S407 is a MEDIUM ZERO adjustment which can select up to 11 positions on a divider string (resistors R443 through R452). Potentiometer R431 is a FINE ZERO adjustment.


FIGURE 16. Meter and Analog Output Circuits.
d. Sensitivity Switching, RANGE Switch S403 has 13 positions which connect resistors R 457 through R469. The range resistors determine the voltmeter gain or sensitivity from 30 microvolts to 30 volts full scale.
e. Power Supply. (As shown on Schematic 21382E). The power for the Model 640 is provided by either a rechargeable 6-volt battery pack or a recitifier circuit operated by $50-60 \mathrm{~Hz}$ line power. Power Switch S301 selects four positions: "AC" (line power), "OrF", "BATT" (battery power) and "BATT TEST" (battery voltage check). The power supply utilizes a -6 volt unregulated voltage from the battery pack or a rectifier circuit composed of transformer T303 secondary (yellow and green taps) and diodes D317-D318. A 5-volt regulator is composed of capacitor C321, transistors Q317Q319 (Darlington series regulator), and reference diode D319. Transistors Q321 and Q322 compose an output sensing amplifier to regulate the series transistor stage. Potentiometer R 338 is an internal adjustment of the regulated output (approximately -5 volts). The regulated voltage is applied to an inverter circuit consisting of transistors Q301-Q302 and saturable core transformer T301.

1. $\pm 40 \mathrm{~V}$ Supply. Power is tapped from a secondary winding on transformer T302 (brown/yellow, brown/white, brown). Diodes D301-D304 and capacitors C302-C303 provide $\pm 40$ volts for the de amplifier output stage.
2.     - 20v Supply. This voltage is not used in the Model 640.
3. $+12 V$ Supply. Power is tapped from a secondary winding on transformer T302 (red/yellow, yellow/ white, yellow). Diodes D307-D310, resistor R304, and capacitor C307 form a rectifier circuit. A voltage doubling circuit consisting of capacitors C305-C306, and diodes D308-D309 forms a bootstrap voltage). Transistors Q303-Q304 form a Darlington series regulator circuit. Feedback is obtained by sampling the - and - 12 volt outputs at the junction of resistors R316 and R317. Transistors Q308 and Q309 form a differential amplifier which senses a change in either the + or - outputs. Another differential pair (transistors Q306-Q307) drives the base of transistor Q304 to complete the feedback loop. Transistor Q305 provides overload-current protection by sensing the current through resistor R305.
4. -12V Supply. Power is tapped from a secondary winding on transformer T302 (red, blue/ white, blue). Diodes D311-D312, resistor R318, and capacitor form a rectifier circuit. Transistors Q310Q311 form a Darlington series regulator circuit. Feedback is obtained by sampling the -12 volt output at the wiper arm of potentiometer R327. This potentiometer adjusts the output voltage. Transistors Q114-Q115 form a differential amplifier with the base of Q314 referenced to diode D314. Trans. istor Q313 drives the base of Q310 to series regulate the output. Transistor Q312 provides overload current protection by sensing the current through resistor R345.
5. Line Power to Battery Switching. The Model 640 can be modified so that a failure of line power (with POWER Switch set to "AC") will cause an automatic switching to battery operation to occur. A diode ( $0.75 \mathrm{~A}, 50 \mathrm{~V}$, Keithley Part No. RF-17) can be connected at the POWER Switch as shown in Figure When line power is present the diode is turned of $f$ and the battery is not used.
f. Battery Charging Circuit. The charging circuit functions whenever the POWER switch is set to "AC" or "OFF". Charging current is provided by a rectifier circuit consisting of diodes D315-D316 and resistor R329. Fuse F302 is rated for $3 / 4$ ampere and used to protect the battery and circuitry during charging or discharging.


FIGURE 17. Line to Battery Switching.
3-5. VOLTAGE FUNCTION. With the FUNCTION Switch set to "VOLTAGE", the Model 640 operates as a sensitive voltmeter with input "OPEN" or shunted by any one of four resistors, R101 through R104.

3-6. CURRENT FAST FUNCTION. With the FUNCTION Switch set to "CURRENT FAST", the Model 640 operates as a feedback ammeter with a Shunt Resistor connected across the amplifier (from High to Feedback). An external resistance can be connected in place of the four Shunt Resistors when switch S102 is set to "OPEN". This method minimizes the slowing effect of capacitance across the input.

3-7. CURRENT INTEGRATE FUNCTION. With the FUNCTION Switch set to "CuRRENT INTEGRATE", the Model 640 operates as a feedback anmeter or coulomb-meter. With a Shunt Resistor connected, (R101 through R104) a 20 pF capacitor (C105) shunts the amplifier to therefore slow the response and filter noisy signals. With switch $\$ 102$ set to "OPEN", capacitor C105 acts as an integrating capacitor for charge or current integration measurements. A simplified diagram of the current integration amplifier is shown in Figure 11. When the FUNCTION Switch is set to "CURRENT INTEGRATE", switch $\$ 402$ connects -5 volts to solenold Kl02 which in turn closes a contact. The contact connects the Damping Control (R108) such that Capacftor C105 is connected in the feedback loop. The Damping Control adjusts the effective capacitance connected in the feedback loop and thus controls the amount of damping. When the Damping Control is adjusted fully clockwise the maximum damping ( 20 pF $\pm .25 \%$ is provided.

## SECTION 4. ACCESSORIES

4-1. GENERAL. The following Kefthley accessories can be used with the Model 640 to provide additional convenience and versatility.

4-2. OPERATING INSTRUCTIONS. A separate Instruction Manual is supplied with each accessory giving complete operating information.

## Mode1 6401 Remote Cable

Description:

The Model 6401 is a shielded coaxial cable with a Keithley CS-195 (male) connector on each end. The cable is 25 feet long.

Application:
The Model 6401 permits remote location of the Input Head up to 25 feet from the Main Chassis with no degradation to the specifications.

Mode 16402 Adapter

## Description:

The Mode1 6402 is special adapter which replaces the UHF adapter supplied with the instrument.

Application:
The Model 6402 adapts the Input Receptacle for GR874 series of coaxial accessories. (General Radio Co.). This adapter is limited to measurements above $10^{-13}$ amperes or source resistances below $10^{14}$ ohms. The adapter can be connected to the Input Head as shown in the illustration.


Model 399 Isolating Amplifier

## Description:

The Model 399 is a unity-gain amplifier which permits operation with the instrument output floated at up to 1500 volts off ground while the Model 399 output is grounded or floated up to 100 volts off ground.

Application:
The Model 399 can be used for "FIFO" operation (floating input, floating output) or when it is necessary to break ground loops within a system. The 1 volt at up to 1 mA output enables use of the Model 399 as a preamp for driving most analog recorders.

## Model 399 Isolating Amplifier (Cont'd.)

Specifications:
GAIN: XI, adjustable $+3 \%$.
GAIN ACCURACY: $\pm 0.2 \%$ (as set at factory).
GAIN LINEARITY: Within 3 millivolts for signal levels below l volt.
FREQUENCY RESPONSE (minimum): Fast: dc to 100 Hz $(-3 \mathrm{~dB})$; Slow: de to $0.3 \mathrm{~Hz}(-3 \mathrm{~dB})$.
NOISE: Less than 5 millivolts $\mathrm{p}-\mathrm{p}, .01 \mathrm{~Hz}$ to 1 kHz ;* less than 0.5 millivolt $\mathrm{p}-\mathrm{p}, .01 \mathrm{~Hz}$ to $0.35 \mathrm{~Hz} . *$
ZERO STABILITY: Better than 3 millivolts/24 hours at reasonably constant ambient temperature.
INPUT RESISTANCE: $10^{6}$ ohms.
INPUT OFFSET CURRENT: Less than $10^{-6}$ ampere.
FULL-SCALE INPUT: $\pm 1$ volt with $100 \%$ overrange.
MAXIMUM INPUT OVERLOAD: 100 volts.
INPUT ISOLATION: Greater than $10^{12}$ ohms at $50 \%$ relative humdiity and $25^{\circ} \mathrm{C}$ shunted by less than 100 picofarads.
MAXIMUM COMMON MODE VOLTAGE: 1500 volts peak, de or ac.
CMRR: Greater than 120 dB at dc , greater than 100 dB up to 1 kHz .
OUTPUT: $\pm$ volt at up to 1 milliampere, $100 \%$ overrange.
OUTPUT ISOLATION: Greater than $10^{8}$ ohms shunted by less than 0.001 microfarad.
POWER: 105-125 or 210-250 volts (switch selected), $50-60 \mathrm{~Hz}, 5$ watts.
DIMENSIONS, WEIGHT: 4-1/2" high $\times 4-1 / 2^{\prime \prime}$ wide $\times 7$ " deep ( $11 \mathrm{~cm} \times 11 \mathrm{~cm} \times 18 \mathrm{~cm}$ ); net weight, 3 pounds ( 1.3 kg ).
ACCESSORIES FURNISHED:
 Model 3991 Input Cable (to safely mate Model 399 to most Keithley instruments).
*Modulation spikes a few hundredths of a volt $\mathrm{p}-\mathrm{p}$ at a $10-\mathrm{kHz}$ rep-rate may be observed with wideband systems.

## Description:

The Model 370 is a compact, paper chart recorder which is compatible with most Keithley instruments having a 1 volt, 1 milliampere output.

Application:
The Model 370 can be used for analog recording applications with inputs floated at up to 500 volts off ground. The Model 3701 Input Cable supplied permits convenient connections to the ingtrument.

Model 370 Recorder


## Description：

The Model 4006 is a rack mounting kit with overall dimensions， 7 inches high x 19 inches wide．Two top covers are provided for use with either 10 inch or 13 inch deep instruments．

## Application：

The Model 4006 converts the instrument from bench mounting to rack mounting．It is suitable for mount－ ing one instrument in one－half of a standard 19－inch rack．

Parts List：

| Item | Qty．Per | Keithley |
| :--- | :--- | :--- |
| No． | Description | Assembly |


| Top Cover， $10^{\prime \prime}$ | 1 | 20016 B |
| :--- | :--- | :--- |
| Panel Adapter Plate | 1 | 19158 A |
| Angle Support | 1 | 19157 A |
| Screw，非10 $\times 3 / 8^{\prime \prime}$ | 4 | $-\ldots-$ |
| Connecting Plate | 1 | 19154 A |
| Screw，非10 x 1／2＂ | 4 | .-- |
| Angle | 1 | 19147 B |
| Top Cover， $13^{\prime \prime}$ | 1 | 20015 B |



Model 4007 Rack Mounting Kit

## Description：

The Model 4007 is a rack mounting kit with overall dimensions， 7 inches high $x 19$ inches wide．Two top

| Item | Qty．Per | Keithley |  |
| ---: | ---: | ---: | ---: |
| No． | Description | Assembly | Part No． | covers are provided for use with either 10 inch or 13 inch deep instruments．

Application：
The Model 4007 converts the instrument from bench mounting to rack mounting．It is suitable for mount－ ing two instruments in a standard 19－inch rack．
Top Cover， $10^{\prime \prime}$
Screw，非10 $\times 1 / 2^{\prime \prime}$
Connecting Plate
Screw，非 $10 \times 1 / 2^{\prime \prime}$
Angle
Top Cover， $13^{\prime \prime}$
Zee Bracket
Plate

20016B
Screw，非10 x 1／2＂

## SECTION 5. SERVICINE

5-1. GENERAL. This section contains procedures for checkout and servicing the instrument. Follow the step-by-step procedures for complete servicing.

5-2. SERVICING SCHEDULE. This instrument requires no periodic maintenance beyond the normal care required for high-quality electronic equipment.

5-3. RARTS REPIACEMENT. Refer to the Replaceable Parts List, Section 7, for information regarding component specifications and part numbers. Replace components as indicated using replacement parts which meet the listed specifications.

5~4. TROUBLESHOOTING.
a. Test Equipment. Refer to Table 5-1 for recommended test equipment for servicing and calibrating this instrument.
b. Troubleshooting Guide. Refer to Table 5-2 for a brief outine of troubleshooting hints. The Table identifies the Symptoms or Trouble, the Probable Cause, and the suggested Solution.

## NOTE

If the instrument problem cannot be readily located or repaired, contact a Keithley representative or the Sales Service Department, Cleveland, Ohio.

TABLE 5-1.
Test Equipment.

| Code <br> Letter | Instrument Type | Specification | Manufacturer and Model No. | Use |
| :---: | :---: | :---: | :---: | :---: |
| A | High Voltage Supply | 0-1000V, .01-V steps, .05\% accuracy. | Keithley, Model 241 | Accuracy checks. |
| B | Nanovolt Source | 10-10 to 1 V , . 25 to $.75 \%$ accuracy. | Keithley, Model 260 | Accuracy checks. |
| C | Picoampere Source | $10^{-4}$ to $10^{-14} \mathrm{~A}$, 25 to $.7 \%$ accuracy. | Keithley, Model 261 | Accuracy checks. |
| D | Megohmmeter | $10^{7}$ to $10^{13}$ ohms $\pm 20 \%$ accuracy. | Keithley, Model 500 | Isolation Resistance Check. |
| E | Differential Voltmeter | 100mV - $500 \mathrm{~V}, .01 \%$ | Keithley, Model 662 | Accuracy checks. |
| F | Digital Voltmeter | $1 \mu \mathrm{~V}$ to $1000 \mathrm{~V}, 0.1 \%$ | Keithley, Model 163 | Trouble-shooting. |
| G | Function Generator | - | Wavetek, Type 110 | Frequency Response Check. |
| H | Oscilloscope | - | Tektronix 503/561A | Trouble-shooting Calibration. |
| I | Probes; 10:1 \& 1:1 | - | Tektronix | Use with Oscilloscope. |
| J | Capacitance Bridge | - | General Radio 1616A | Capacitor checks. |
| K | Variable Transformer \& Power Line Meter | $\bullet$ | Variac/RCA | Power Supply Calibration. |
| L | Recorder | lmA sensitivity; . 05 s Rise Time 10-90\% | Keithley, Model 370 | Drift and Noise Checks. |

TABLE 5-2.
Troubleshooting Guide.

| Symptom or Trouble | Probable Cause | Solution | $\begin{gathered} \text { Sub- } \\ \text { Assembly } \end{gathered}$ | Figure |
| :---: | :---: | :---: | :---: | :---: |
| Excessive Voltage Drift | Vibrating Capacitor | Replace V.C. (C121). | INPUT HEAD | - |
|  | Meter Zero Circuit | Check diodes D405-6 and potentiometer R431. | PC-149 | 23 |
|  | DC Amplifier | Check bias voltages. | PC-150 | 25 |
| Excessive Noise at OUTPUT or Meter | Vibrating Capacitor | Replace V.C. (C121). | INPUT HEAD | - |
|  | Input FET (Q101) | Replace FET (Q101). | PC-151 | 24 |
| Excessive Current Offset or drift | Vibrating Capacitor | Replace V.C. (C121). | INPUT HEAD | - |
|  | Defective Insulation | Check sapphire insulation. | INPUT HEAD | - |
|  | Excessive Humidity | Allow instrument to warm-up. $\mathrm{Re}-$ activate the dessicant in the INPUT HEAD. | INPUT HEAD | - |
| Response Time Slow | Vibrating Capacitor | Calibrate drive circuit as in para. 6-3. | - | - |
|  | Power Supplies | Check voltages in the INPUT HEAD. | INPUT HEAD | - |
|  | AC Amplifier | Check for proper gain. | PC-151 | 24 |
|  | Oscillator Circuit | Check drive voltages. Calibrate as in para. 6-3. | PC-247 | 27 |
| Meter Pegs Off-Scale (all ranges) | Power Supplies | Check voltages on the Main Chassis. | $\begin{aligned} & \mathrm{PC}-148, \\ & \mathrm{PC}-149 \end{aligned}$ | $\begin{aligned} & 18 \\ & 19 \end{aligned}$ |
|  | DC Amplifier | Check meter circuit. | PC-150 | 25 |
|  | Vibrating Capacitor | Replace V.C. (Cl21). | INPUT HEAD | - |
| (one range only) | RANGE Resistor | Check RANGE switch. Replace RANGE resistors. | S403 | - |



FIGURE 18. Test Points, PC-148.


FIGURE 19. Test Points, PC-149.


FIGURE 20. Chassis, Top View.


FIGURE 21. Chassis, Top View.


FIGURE 22. Component Layout, PC-148.


FIGURE 23. Component Layout, PC-149.


FIGURE 24. Component Layout, PC-151.


FIGURE 25. Component Layout, PC=150.


FIGURE 26. Component Layout, PC-153.


FIGURE 27. Component Layout, PC-247.

5-5. CHECKOUT PROCEDURE, Refer to Table 5-3 for step-by-step procedures for instrument checkout.

## NOTE

Before a step-by-step checkout is started, inspect the circuits visually to detect problems such as broken wire, loose parts, dirty or oily switch contacts, etc.

WARNING
Use care when troubleshooting an instrument connected to line power and/or with Power switch on. Whenever resistance checks are made, remove all power to instrument and discharge power supply capacitors through a low value resistor (1002).

TABLE 5-3.
Checkout Procedure.

| Para. $15-5$ | Description | SubAssembly | Figure | Test <br> Point | Circuit Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a. | Connect the shorting link between GND and LO on rear panel of Model 640. | Main Chassis | 4 | Rear Panel | - |
| b. | Place Dust Cover (20911A) over Input receptacle (To prevent contamination and stray noise pickup) | INPUT HEAD | - | - | - |
| c. | Check retaining screws on all PC boards in the INPUT HEAD. (The LO to case connection is made through these screws). | INPUT HEAD | - | - | - |
| d. | Check the unregulated voltage on PC-148. Voltage should be nominal-11 volts dc with 3 volts $\mathrm{p}-\mathrm{p}$ ripple. Use Oscilloscope (H). | PC-148 | 18 | -11V Unreg. | Para. 3-4e |
| e. | Check the regulated voltage on $\mathrm{PC}-148$. Voltage should be nominal -5 volts. | PC-148 | 18 | -5V | Para. 3-4e |
| f. | Check inverter voltage on PC-148. Voltage should be 5 V p-p square wave at 1100 Hz . | PC-148 | 18 | Inverter | Para, 3-4e |
| g. | Check the $\pm 40 \mathrm{~V}$ unregulated voltages on PC-149. | PC-149 | 19 | $\pm 40 \mathrm{~V}$ | Para. 3-4e |
| h. | Check the unregulated voltage at collector of Q303. Voltage should be nominal 15 volts dc. | PC-149 | 19 | +15V Unreg. | Para. 3-4e |
| 1. | Check regulated +12 V on PC-149. | PC-149 | 19 | +12V | Para. 3-4e |
|  | Check regulated -12 V on $\mathrm{PC}-149$. | PC-149 | 19 | -12V | Para. 3-4e |
|  | If all power supply voltages are nominal proceed to oscillator check. | - | - | - | - |
| 1. | Check Vibrating Capacitor drive signal on PC247. | PC-247 | 27 | - | Para. 3-3e |
| m. | Check demodulator drive signal on PC-247. | PC-247 | 27 | - | Para. 3-3e |
|  | Check the dc amplifier circuit on PC-150. | PG-150 | 25 | - | Para, 3-4a |
| p. | Check meter circuit on $\mathrm{PC}-149, \mathrm{PC}-150$. | $\begin{aligned} & \mathrm{PC}-149, \\ & \mathrm{PC}-150 \end{aligned}$ | $\begin{aligned} & 23 \\ & 25 \end{aligned}$ | - | Para. 3-4b |

## SECTION 6. CALIBRATION

6-1. GENERAL. This section contains procedures for checking the instrument in order to verify operation within specifications.

6-2. TEST EQUIPMENT. Refer to Table 5-1 for recommended test equipment for servicing and calibrating this instrument.

6-3. CALIBRATION PROCEDURE. Refer to Table 6-1 for step-by-step procedures for calibrating this instrument.

NOTE

If proper facilities and equipment are not available, contact a Keithley representative or the Sales Service Department, Cleveland, Ohio. Keithley Instruments, Inc. maintains a complete repair and calibration facility with equipment traceable to the National Bureau of Standards.

TABLE 6-1.
Calibration Procedures.

| Para. $6-3$ | Specification or Adjustment | Description | Measurement | SubAssembly | Figure | Test Point |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a. | LO to GND Isolation | Set Power to "OFF". Remove shorting link between GND and 10 on rear pane1. Measure LO to GND resistance using Megohmmeter (D). | LO to GND should be greater than $10^{9} \Omega$. | Main <br> Chassis | 4 | LO to GND |
| b. | Mechanical Zero Adjust | Set meter zero. | - | Main <br> Chassis | 2 | Meter |
| c. | Line Voltage Setting | Connect Variac and set line voltage for 115 V . | 115 V nominal. |  |  |  |
| d. | -5V Reg. Voltage | Set Power to "AC" Measure -5V Supply on PC-148 using Diff. Voltmeter (F). | Adjust potentiometer R338 for $-5 \mathrm{~V} \pm 5 \mathrm{mV}$. | PC-148 | 22 | - |
| e. | Ripple Voltage | Measure ripple on $-5 V$ supply using Oscilloscope (H). | Ripple to be less than $500 \mathrm{mV} \mathrm{p}-\mathrm{p}$. | PC-148 | $\begin{aligned} & 18 \\ & 22 \end{aligned}$ | - |
| f. | Voltage Checks | ```Check remaining voltages. -12V Supply. (Ripple should not exceed 5mV p-p).``` | Adjust potentiometer R327 for $-12 \mathrm{~V}, \pm 5 \mathrm{mV}$. |  |  |  |
|  |  | +12 V Supply. (Ripple should not exceed $15 \mathrm{mV} \mathrm{p}-\mathrm{p}$ ). | $+12 \mathrm{~V} \pm 500 \mathrm{mV}$ | PC-149 | $\begin{aligned} & 19 \\ & 23 \end{aligned}$ | - |
|  |  | -40V Supply, (Ripple should not exceed $50 \mathrm{mV} p-\mathrm{p}$ ). | $-40 \mathrm{~V} \pm 2 \mathrm{~V}$ | PC-148 | $\begin{aligned} & 18 \\ & 22 \end{aligned}$ | - |
|  |  | +40V Supply. (Ripple should not exceed $50 \mathrm{mV} p-p$ ). | $+40 \mathrm{~V} \pm 2 \mathrm{~V}$ | PC-148 | $\begin{aligned} & 18 \\ & 22 \end{aligned}$ | - |
| g. | Zero Circuit | Check zener voltage on PC-149 using Diff. Voltmeter (E). | ```D405 voltage should be +9V }\pm5 Noise less than 0.3mV``` | PC-149 | 23 | - |
|  |  | Check zener voltage on PC-149 using Diff. Voltmeter (E). | ```D406 voltage should be -9V +5%. Noise less than 0.3mV.``` | PC-149 | 23 | - |

TABLE 6-1. (cont'd)
Calibration Procedures.

| Para. $6-3$ | Specification or Adjustment | Description | Measurement | SubAssembly | Figure | Test <br> Point |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| h. | Battery Charging Circuit | Set Power to "OFF". With line cord connected measure the charging voltage at R329. | Voltage should be -22 V with less than 27 V p-p ripple. | Main Chassis | - | R329 |
| 1. | Battery Check | Set POWER Switch to "BATT TEST". | Meter should indicate greater than 6 V . | Main <br> Chassis | - | Meter |
| J. | Oscillator Check | Check wave form on PC-247 using Oscilloscope (H). <br> NOTE: Use a 10:1 Probe for the Oscilloscope input. Use $1: 1$ Probe for EXT TRIGGER and connect to R521 (wiper). | See Figure 28 for desired wave form. | PC-247 | $\begin{aligned} & 27 \\ & 28 \end{aligned}$ | Oscillator Wave form J104 R521 |
| k. | Oscillator Recovery | Set Power to "OFF" for 10 seconds. When Power is set to "AC" the Oscillator signal should recover. | - | - | - | - |
| 1. | Oscillator <br> Adjustment | Adjust variable capacitor C502 to "start" oscillator if necessary. <br> Set the Gain Adjust potentiometer R506 to obtain a stable waveform. | - | PC-247 | 27 | C502 |
| m. | Symmetry Adjustment | Set the Sym. Adjust potentiometer R521 for equal demodulator "ON" and "OFF" times. | See Figure 29. | PC-247 | $\begin{aligned} & 27 \\ & 28 \end{aligned}$ | R521 |
| n. | Phase Adjustment | Set Phase Adjust potentiowater R517 for proper phasing as shown in Fig. 30. Note: The amplifier must be driven into saturation to obtain a phase pattern. | See Figure 30 for phasing. | PC-247 | $\begin{aligned} & 27 \\ & 29 \end{aligned}$ | R517 |
| $p$. | Unity Gain Check | Set Funcision to vOLTAGE <br> RANGE to IVOLT <br> Neter to " + " <br> POWER to AC <br> SHUNT RESISTOR to $10^{6}$ <br> Connect the Nanovolt Source (B) to the Model 640 Input using UHF adapter. Connect the Differential Voltmeter to read the difference potential between the Input high and PEEDBACK terminals of the Model 640. With the Nanovolt Source set to 0-00 , adjust the Model 640 zero controls for null on the Diff. Voltmeter ( $+10 \mu \mathrm{~V}$ ). Apply +1.000 V to Model 640 and check the Diff. Voltmeter null. The Diff. Voltmeter should indicate within +100 microvolts. | $\sim$ | INPUT HEAD |  | FEEDBACK <br> Terminal on INPUT HEAD |

TABLE 6-1. (cont'd)
Calibration Procedures.

| Para. $6-3$ | Specification or Adjustment | Description | Measurement | SubAssembly | Figure | Test Point |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| q. | Meter Cal. for Full Scale | Set front panel controls as in 6-3p. Apply +1 volt using Nanovolt Source (B). | Input +1.000 V | - |  | - |
|  |  | Observe the Model 640 OUTPUT using Diff. Voltmeter. | OUTPUT should be $+1.000 \mathrm{~V} \pm$ 10 mV . | - |  | - |
|  |  | Adjust Meter Cal potentiometer R455 for full scale deflection. |  | PC-147 | 20 | R455 |
| r. | Meter Cal. for Center Scale | Without readjusting the Zero controls set the Meter for Center Scale. Adjust the Center Zero potentiometer R42l for zero while in ZERO CHECK mode. | - | PC-147 | 20 | R421 |
| $s$. | Voltage Range Accuracy Check | Set front panel controls as in 6-3 p. Check all voltage ranges for full scale accuracy. Use the Nanovolt Source as input reference. | Accuracy to be $\pm 1 \%$ of full scale on $30 \mathrm{~V}-300 \mu \mathrm{~V}$ ranges. $\pm 5 \%$ on the $30 \mu \mathrm{~V}$ range. | - | - | - |
| t. | Meter Noise | Set front panel controls as in 6-3 p. Place Dust Cap over the Input. | - | - | - | - |
|  |  | Observe Meter Noise on the $30 \mu \mathrm{~V}$ Range. | Meter Noise to be less than $2 \mu \mathrm{~V} p$. | - | $\checkmark$ | - |
| u. | OUTPUT Noise | Observe OUTPUT Noise using Oscilloscope (H). | OUTPUT noise to be less than 100 mV p-p, however occasional spikes may exceed 100 mV . | - | - | - |
| v. | Current Range Accuracy ( $10^{6} \Omega$ Shunt) | Set RANGE to 10 V <br> FUNCTION to CURRENT FAST <br> METER to " + " <br> POWER to "AC" <br> SHUNT RESISTOR to $10^{6}$ <br> Check the OUTPUT accuracy with the Picoampere Source (C) used as In* put current reference. | Accuracy should be $\pm 3 \%$ of full scale. | - | - | - |
|  |  | RANGE CURRENT <br> 10 V $10^{-5} \mathrm{~A}$ <br> 1 V $10^{-6 \mathrm{~A}}$ <br> 100 mV $10^{-7} \mathrm{~A}_{\mathrm{A}}$ <br> 10 mV $10^{-8} \mathrm{~A}$ <br> 1 mV $10^{-9} \mathrm{~A}$ |  |  |  |  |
| W. | Current Range Accuracy ( $10^{8} \Omega$ Shunt) | Verify OUTPUT accuracy as in $6-3$ v. with SHUNT RESISTOR set to $10^{8}$ and RANGE to 1 V . | Accuracy should be $\pm 3 \%$ of $10^{-8} \mathrm{~A}$ full scale. | - | - | - |

TABLE 6-1. (cont'd)
Calibration Procedures.

| $\begin{aligned} & \text { Para. } \\ & 6-3 \end{aligned}$ | Specification or Ad justment | Description | Measurement | SubAssembly | Figure | Test Point |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x$. | Current Range Accuracy ( $10^{10} \Omega$ Shunt) | Verify OUTPUT accuracy with SHUNT RESISTOR set to $10^{10}$ and RANGE to 1V. | Accuracy should be $\pm 3 \%$ of full scale. | - | - | - |
|  |  | Repeat above using 10 mV RANGE. $\left(10^{-12} \mathrm{~A}\right)$. | Accuracy should be $\pm 4 \%$ of full scale. | - | - | - |
| y. | ```Current Range Accuracy (1012\Omega Shunt)``` | Verify OUTPUT accuracy with SHUNT RESISTOR set to $10^{12}$ and RANGE to IV. | Accuracy should be $\pm 4 \%$ of full scale. | - | - | - |
| 2. | Current Rise Time | Set RANGE to 1 V <br> FUNCTION to CURRENT INTEGRATE <br> METER to OFF <br> POWER to AC <br> SHUNT RESISTORS to $10^{12}$ <br> Set Damping to MAX: Apply $+10^{-12}$ A input current using Picoampere source. Observe $10-90 \%$ rise time using oscilloscope. | 10-90\% Rise Time to be less than 44 sec . | - | - | - |
| aa. | Frequency Response | Set RANGE to 10 mV <br> FUNCTION to VOLTAGE <br> METER to OFF <br> POWER to AC <br> SHUNT RESISTOR to $10^{6}$ | - | - | - | - |
|  |  | Apply 10 Hz sinewave to Input using Function Generator (G). Adjust signal for $1.6 \mathrm{~V} \mathrm{p}-\mathrm{p}$ as observed at OUTPUT using Oscilloscope (H). | - | - | - | - |
|  |  | Set Function Generator (G) for 1 Hz . | OUTPUT should remain at 1.6 V p-p. | - | - | - |
|  |  | Increase the frequency of Function Generator until OUTPUI is reduced to $1.1 \mathrm{~V} p-\mathrm{p}$. ( 3 dB down). | Frequency at 3 dB down should be 35 Hz or higher. | - | - | - |
| bb. | Drift Check | NOTE: The Model 640 power must be off for at least 2 hours prior to this check. Connect Recorder (L) to the Model 640 OUTPUT. With Dust Cover in place allow a 60 minute warm-up. <br> Set RANGE to 100 MICROVOLTS <br> FUNCTION to VOLTAGE <br> SHUNT to $10^{6}$ | - | - | - | - |
|  |  | NOTE: Maintain a constant ambient temperature if possible. Otherwise monitor temperature change to compensate for $35 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ drift. |  |  |  |  |
|  |  | After warm-up period the drift should not exceed $35 \mu \mathrm{~V}$ per 24 hours. | Drift less than $35 \mu \mathrm{~V}$ per 24 hours. | - | - | - |



FIGURE 28. Typical Oscillator Waveform.


FIGURE 29. Proper Symmetry Adjustment.


FIGURE 30. Proper Phase Adjustment.

## SECTION 7. REPLACEABLE PARTS

7-1. REPLACEABLE PARTS LIST: This section contains a list of components used in this instrument for user reference. The Replaceable Parts List describes the individual parts giving Circuit Designation, Description, Suggested Manufacturer (Code Number),

Manufacturer's Part Number, and the Keithley Part Number. Also included is a Figure Reference Number where applicable. The complete name and address of each Manufacturer is listed in the CODE-TO-NAME Listing following the parts list.

TABLE 7-1.
Abbreviations and Symbols

| A | ampere | $\begin{aligned} & F \\ & F i g \end{aligned}$ | farad <br> Figure | $\Omega$ | ohm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CbVar | Carbon Variable |  |  | p | pico ( $10^{-12 \text { ) }}$ |
| Cerd | Ceramic Disc | GCb | Glass enclosed Carbon | PC | Printed Circuit |
| Cer Trimmer | Ceramic Trimmer |  | kilo (10 ${ }^{3}$ ) | Poly | Polystyrene |
| Comp | Composition | k | kilo (10 ${ }^{3}$ ) | Ref. | Reference |
| DCb | Deposited Carbon | $\mu$ | micro ( $10^{-6}$ ) |  |  |
| Desig. | Designation | M | $\operatorname{Meg}\left(10^{6}\right)$ | TCu | Tinner Copperweld |
| EAL | Electrolytic, Aluminum | Mfr. | Manufacturer | V | volt |
| ETB | Electrolytic, tubular | MtF | Metal Film |  |  |
| ETT | Electrolytic, tantalum | My | Mylar | W WW | watt |
|  |  | No. | Number | WWVar | Wirewound Variable |

7-2. ELECTRICAL SCHEMATICS AND DIAGRAMS. Schematics and diagrams are included to describe the electrical circuits as discussed in Section 3. Table 7-2 identifies all schematic part numbers included.

7-3. HOW TO USE THE REPLACEABLE PARTS LIST. This Parts List is arranged such that the individual types of components are listed in alphabetical order. Main Chassis parts are listed followed by printed circuit boards and other subassemblies.

7-4. HOW TO ORDER PARTS.
a. Replaceable parts may be ordered through the

Sales Service Department, Keithley Instruments, Inc. or your nearest Keithley representative.
b. When ordering parts, include the following information.

1. Instrument Model Number.
2. Instrument Serial Number.
3. Part Description.
4. Schematic Circuit Designation.
5. Keithley Part Number.
c. All parts listed are maintained in Keithley Spare Parts Stock. Any part not listed can be made available upon request. Parts identified by the Keithley Manufacturing Code Number 80164 should be ordered directly from Keithley Instruments, Inc.
table 7-2.

| Description | Circuit Designation | Schematic Part No. |
| :---: | :---: | :---: |
| Remote Head | PC-151, PC-153, PC-247, PC-249 | 21381 E |
| Power Supply | PC-147, PC-148, PC149 | 21382 E |
| Switching (Main Chassis) | PC-150 | 21383 E |

TABLE 7-3.
Gircuit Designation Series.

| Series | Description | Circuit Desig. | Page No. |
| :---: | :---: | :---: | :---: |
| 100 | Remote Head, Amplifier | PC-151, PC-153, PC-249 | 44 |
| 200 | - | PC-153 | - |
| 300 | Power Supply | PC-147, PC-148, PC-149 | 41 |
| 400 | Main Chassis | PC-150 | 38 |
| 500 | Remote Head, Oscillator | PC-247 | 47 |

TABLE 7-4.
Mechanical Parts List.



FIGURE 31. Top Cover Assembly.


FIGURE 32. Bottom Cover Assembly.

MAIN CHASSIS PARTS LIST
(Refer to Schematic 21383 E for circuit designations).

## CAPACITORS

| Circuit <br> Desig. | Value |  | Rating |  | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C401 | . 82 | $\mu \mathrm{F}$ | 20 | V | ETT | 05397 | KOR27J20K | C80-.82M | 25 |
| C402 | 4.7 | $\mu \mathrm{F}$ |  | V | ETT | 05397 | K4R7J20K | C80-4.7M | 25 |
| C403 | 4.7 | $\mu \mathrm{F}$ | 20 | V | ETT | 05397 | K4R7J20K | C80-4.7M | 25 |
| C404 | . 1 | $\mu \mathrm{F}$ | 200 | V | My | 02777 | P12M-C | C47-.1M | - |
| C405 | . 05 | $\mu F$ | 600 | V | My | 56289 | 6PS-S50 | C62-.05M | 20 |

*Nominal

DIODES

| Circui Desig. | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D401 | Zener | 12954 | 1N709 | DZ-21 | 25 |
| D402 | Silicon | 01295 | 1N645 | RF-14 | 25 |
| D403 | Silicon | 01295 | 1N645 | RF-14 | 25 |
| D404 | Zener | 12954 | 1N715 | DZ-22 | 20 |
| D405 | Zener | 04713 | 1 N 936 | 02-5 | 23 |
| D406 | Zener | 04713 | 1N936 | D2-5 | 23 |
| D407 | Zener | 12954 | 1N706 | DZ-1 | 25 |

MISCELLANEOUS PARTS

| Circuit Desig. | Description | Mfr. Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3401 | Connector, 9 pin card-edge | 03612 | PSC4SS9 | CS-175-9 | 20 |
| J402 | Binding Post | 05474 | DF21B | BP-11B | 20 |
| J403 | Binding Post, FEEDBACK | 58474 | DF21blu | BP-118LU | 20 |
| J404 | Receptacle, Microphone, OUTPUT | 02660 | 80 PC 2 F | CS-32 | 4 |
| -- | Plug, Microphone, mate of 3404 | 02660 | 80 PC 2 M | CS-33 | - |
| J405 | Connector, Receptacle | 02660 | 5740240 | CS-196 | 4 |
| P402 | Connector, mate of J 405 | 02660 | --- | CS-195 | - |
| J406 | Binding Post, GND | 58474 | DF21G | BP-11G | 20 |
| --- | Shorting Link | 24655 | 938L | BP-6 | 4 |
| S401 | Push Button Switch, ZERO CHECK | 80164 | --- | SW-223 | 2 |
| --- | Knob Assembly, Zero Check | 80164 | --- | 16373A | 2 |
| S402 | Rotary Switch less components, FUNCTION | 80164 | --- | SW-227 | 2 |
| --- | Dial Assembly, Function Switch | 80164 | --- | 14838A | 2 |
| S403 | Rotary Switch less components, RANGE | 80164 | --- | SW-228 | 2 |
| --- | Rotary Switch with components, Range | 80164 | --- | 21336B | 2 |
| --- | Dial Assembly, Range Switch | 80164 | --- | 21200A | 2 |
| S404 | Rotary Switch less components, METER | 80164 | --- | SW-225 | 2 |
| --- | Dial Assembly, Meter Switch | 80164 | --- | 14838A | 2 |
| S405 | Rotary Switch less components, COARSE zero | 80164 | --- | SW-224 | 4 |
| - | Rotary Switch with components, Coarse Zero | 80164 | -** | 21361 B | 4 |
| -- | Knob Assembly, Coarse Zero Switch | 80164 | --- | 16373A | 4 |
| --- | FINE ZERO Control (R431) | 80164 | 62JA-1K-2W | RP42-1K | 2 |
| --- | Knob Assembly, Fine Zero | 80164 | --- | 16994A | 2 |

MAIN CHASSIS (cont'd)
MISCELLANEOUS (cont'd)

| Circuit Desig. | Description | Mfr. <br> Code | $\begin{aligned} & \text { Mfr. } \\ & \text { Part No. } \\ & \hline \end{aligned}$ | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S406 | Slide Switch, IV-IMA | 80164 | --- | SW-45 | 4 |
| S407 | Rotary Switch less components, MEDIUM ZERO | 80164 | --- | SW-209 | 4 |
| --- | Rotary Switch with components, Medium Zero | 80164 | --- | 21335B | 4 |
| --- | Dial Assembly, Medium Zero Switch | 80164 | --- | 16993A | 4 |
| --- | 1 MA CAL Control (R423) | 71450 | AW-20K-5W | RP34-20K | 4 |
| --- | Knob Assembly, 1 Ma Cal Control | 80164 | --- | 16373A | 4 |
| M401 | Meter | 80164 | -- | ME-71 | 20 |

RESISTORS

| Circult <br> Desig. | Value | Rating | Type | Mfr. Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R401 | $500 \mathrm{k} \Omega$ | 10\%, 1/2 W | DCb | 00327 | N11A | R12-500K | 25 |
| R402 | $68 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-68K | 25 |
| R403 | $68 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-68K | 25 |
| R404 | $2 \mathrm{k} \Omega$ | 1/4 W | Cb | 09569 | MTC23Ll | RP59-2K | 25 |
| R405 | $50 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N1 1A | R12-50K | 25 |
| R406 | $10 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-10K | 25 |
| R407 | $12 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-12K | 25 |
| R408 | $560 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-560 | 25 |
| R409 | $12 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-12K | 25 |
| R410 | $27 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-27K | 25 |
| R411 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-100K | 25 |
| R412 | $1 \mathrm{M} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-1M | 25 |
| R413 | $39 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-39k | 25 |
| R414 | $150 \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-150 | 25 |
| R.415 | $120 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | RL-120K | 25 |
| R416 | 35 k ת | 1\%, 1/2 W | DCb | 00327 | N11A | R12-35K | 25 |
| R417 | $820 \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-820 | 25 |
| R418 | $3 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-3K | 25 |
| R419 | $20 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-20k | 20 |
| R420 | $15 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N1 1 A | R12-15K | 20 |
| R421 | $10 \mathrm{k} \Omega$ | 20\%, 2 W | WW | 71450 | INS 115 | RP50-10K | 20 |
| R422 | $910 \Omega$ | 0.5\%, 1/2W | MtF | 07716 | CEC | R61-910 | - |
| R423 | 20 kS | 10\%, 5 W | WWVar | 71450 | AW | RP34-20K | 20 |
| R424 | 8.6 k $\Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-8.6K | 20 |
| R425 | $1.5 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R58-1.5K | 23 |
| R426 | $1.5 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R 58 -1.5K | 23 |
| R427 | $11 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R58-11K | 23 |
| R428 | $11 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R58-11K | 23 |
| R429 | $80 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R58-80 | 20 |
| R430 | $80 \mathrm{k} \Omega$ | 1\%, 1/2 W | WW | 01686 | E-30 | R58-80 | 20 |
| R431 | $1 \mathrm{k} \Omega$ | 5\%, 2 W | wWVar | 12697 | 62JA | RP42-1K | 20 |
| R432 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R433 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R434 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R435 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3W | WWenc | 01686 | 7010 | R105-1.11K | 20 |

MAIN CHASSIS (cont'd) RESISTORS (cont'd)

| Circuit Desig. | Value | Rating | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R436 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3 W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R437 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3 W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R438 | $1.11 \mathrm{k} \Omega$ | $1 / 4 \%, 1 / 3 \mathrm{~W}$ | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R439 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3 W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R441 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3 W | WWenc | 01686 | 7010 | R105-1.11K | 20 |
| R442 | $1.11 \mathrm{k} \Omega$ | 1/4\%, 1/3 W | WWenc | 01686 | 7010 | R105-1,11K | 20 |
| R443 | 320 ת | 0.1\%, 1/2 W | WW | 15905 | 1142 | R67-320 | - |
| R444 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R445 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R446 | $320 \Omega$ | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R447 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R448 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R449 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R450 | 320 ת | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R451 | $320 \Omega$ | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R452 | $320 \Omega$ | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| $R 453$ | $320 \Omega$ | 0.1\%, 1/2 W | WW | 15909 | 1142 | R67-320 | - |
| R454 | $9.7 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-9.7K | * |
| R455 | $2 \mathrm{k} \Omega$ | 20\%, 2 W | WW | 71450 | 1NS 115 | RP50-2K | 20 |
| R456 | $500 \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-500 | - |
| R457 | $27.3 \mathrm{k} \Omega$ | 0.5\%, 1/2 W | MtF | 07716 | CEC | R61-27.3K | - |
| R458 | $9.1 \mathrm{k} \Omega$ | 0.5\%, 1/2 W | MtF | 07716 | CEC | R61-9.1K | - |

TRANSISTORS

| Circuit Desig. |  | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. |  | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Q401 | N-Channel FET, Case TO-92 | 01295 | SF5043 | TG-40 | * | 25 |
| Q402 | N-Channel FET, Case TO-92 | 01295 | SF5043 | TG-40 |  | 25 |
| Q403 | PNP, Case R-110 | 07263 | S17638 | TG-33 |  | 25 |
| Q404 | PNP, Case R-110 | 07263 | S17638 | TG-33 |  | 25 |
| Q405 | N -Channel FET, Case TO-92 | 04713 | MPF 103 | TG-41 |  | 25 |
| Q406 | NPN | 73445 | A1380 | TG-32 |  | 25 |
| Q407 | NPN | 80164 | --. | 21676A |  | 25 |
| Q408 | PNP | 02735 | 2N398A | TG-13 |  | 25 |
| Q409 | NPN | 80164 | --- | 21676A |  | 25 |

[^0]POWER SUPPLY PARTS
(Refer to Schematic No. 21382 E for circuit designations).

| Circuit Desig. | Value | Rating | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C301 | . 01 HF | 200 V | My | 13050 | SM1A | C47-.01M | 22 |
| C302 | $50 \mu \mathrm{~F}$ | 50 V | ETT | 37942 | TC39 | C39-50M | 22 |
| C303 | $50 \quad \mu \mathrm{~F}$ | 50 V | ETT | 37942 | TC39 | $\mathrm{C} 39-50 \mathrm{M}$ | 22 |
| C304 | Not Used |  |  |  |  |  |  |
| C305 | $100 \mu \mathrm{~F}$ | 25 V | EAL | 56289 | 89D226 | C94-100M | 23 |
| C306 | $50 \quad \mu \mathrm{~F}$ | 50 V | ETT | 37942 | TC39 | C39.50M | 23 |
| C307 | 100 HF | 25 V | EAL | 56289 | 89D226 | C94-100M | 23 |
| C308 | Not Used |  |  |  |  |  |  |
| C309 | 330 pF | 1000 V | CerD | 71590 | DD331-10\% | C22-330P | 23 |
| C310 | $2.2 \mu \mathrm{~F}$ | 50 V | ETB | 05397 | J2R2J50S | C149-2. 2 M | 23 |
| C311 | . 02 LF | 1000 V | CerD | 56289 | 10SS-S20 | C22-.02M | 23 |
| C312 | . $0022 \mu \mathrm{~F}$ | 1000 V | CerD | 72982 | $811000 \times 5$ F0222 | C22.0022M | 23 |
| C313 | . $01 \mu \mathrm{~F}$ | 600 V | Cerd | 56289 | 10SS-S10 | C22-.01M | 23 |
| C314 | $100 \mu \mathrm{~F}$ | 25 V | EAL | 56289 | 89 D 226 | C94-100M | 23 |
| C315 | $100 \mu \mathrm{~F}$ | 25 V | EAL | 56289 | 89D226 | C94-100M | 23 |
| C316 | Not Used |  |  |  |  |  |  |
| C317 | Not Used |  |  |  |  |  |  |
| C318 | . $02 \mu \mathrm{~F}$ | 1000 V | CerD | 56289 | 10SS-S20 | C22-.02M | 23 |
| C319 | . 01 WF | 1000 V | CerD | 56289 | 10SS-S10 | C22-.01M | 23 |
| C320 | 100 HF | 25 V | EAL | 56289 | 89D226 | C94-100M | 23 |
| C321 | $500 \mu \mathrm{~F}$ | 25 V | EAL | 24309 | JC8100258P | C211-500M | 22 |
| C322 | . 0033 嗗 | 1000 V | CerD | 56289 | 10SS-D33 | C22-. 0033 M | 22 |
| C323 | 500 HF | 25 V | EAL | 56289 | JC8100258P | C211-500M | 22 |
| C324 | *100 $\mu \mathrm{F}$ | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | - |

*Nominal
DIODES

| Circuit <br> Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D301 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D302 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D303 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D304 | Sillcon | 01295 | 1N645 | RF-14 | 22 |
| D305 | Not Used |  |  |  |  |
| D306 | Not Used |  |  |  |  |
| D307 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D308 | Silicon | 01295 | 1N645 | RF-14 | 23 |
| D309 | Silicon | 01295 | 1N645 | RF-14 | 23 |
| D310 | Silicon | 01294 | 1N645 | RF-14 | 23 |
| D311 | Silicon | 01295 | 1N645 | RF-14 | 23 |
| D312 | Silicon | 01295 | 1N645 | RF-14 | 23 |
| D313 | Silicon | 01295 | 1N645 | RF-14 | 23 |
| D314 | Zener | 04713 | 1N935 | D2-7 | 23 |
| D315 | Silicon | 01295 | 1N645 | $\mathrm{RF}-14$ | 22 |
| D316 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D317 | Sticon | 02735 | 1N3256 | RF-22 | 22 |
| D318 | Silicon | 02735 | 1N3256 | RF-22 | 22 |
| D319 | Zener | 12954 | 1N709 | D2-21 | 22 |
| D320 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D321 | Silicon | 01295 | 1N645 | RF-14 | 22 |
| D322 | Zener | 12954 | 1N709 | DZ-21 | 22 |
| D323 | Silicon | 01295 | 1N645 | RF-14 | 20 |


| Circuit Desig. | Description | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BT301 | Battery Assembly | 80164 | --- | 23731A | 20 |
| F301 (217V) | Fuse, .25A, 3 Ag | 75915 | 313.250 | FU-17 | - |
| F301 (234V) | Fuse, . 125A, slow blow | 71400 | MDL | FU-20 | - |
| F302 | Fuse, Battery, 1A, 3 AG | 75915 | 312001 | FU-7 | - |
| --- | Fuse Holder | 75915 | 34201 | FH-3 |  |
| --- | Fuse Holder | 75915 | 346001 | EH-9 |  |
| P301 | Cord Set | 80164 | --- | CO-5 | 4 |
| S301 | Rotary Switch less components, POWER | 80164 | --- | SW-226 | 2 |
| --- | Rotary Switch with components, POWER | 80164 | --- | 21337B |  |
| --- | Dial Assembly, POWER Switch | 80164 | --- | 18393A | - |
| S302 | Slide Switch, 117-234 V | 80164 | --- | SW-151 | 4 |
| J301 | Connector, PC board 1.48 | 03612 | PSC4SS2212 | CS-182-9 | 20 |
| J302 | Connecto PC board 149 | 03612 | PSC4SS2212 | CS-182-2 | 20 |
| T301 | Transformer | 80164 | --- | TR-102 | - |
| T302 | Transformer | 80164 | --- | TR-101 | 20 |
| T303 | Transformer | 80164 | --- | TR-110 | 20 |

RESISTORS

| Circuit <br> Desig. | Value | Rating | Type | Mfr. Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R301 | 47 ת | 10\%, 1/2 W | Comp | 01121 | EB | Rl-47 | 22 |
| R302 | 470 ת | 10\%, 1/2 W | Comp | 01121 | EB | R1-470 | 22 |
| R303 | $10 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-10K | 23 |
| R304 | $10 \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-10 | 23 |
| R305 | $4.7 \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | Rl-4.7 | 23 |
| R306 | $4.7 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-4.7K | 23 |
| R307 | Not Used |  |  |  |  |  |  |
| R308 | 47 k ת | 10\%, 1/2 W | Comp | 01121 | EB | R1-47K | 23 |
| R309 | Not Used |  |  |  |  |  |  |
| R310 | $100 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-100K | 23 |
| R311 | $27 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-27K | 23 |
| R312 | $47 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-47K | 23 |
| R313 | $47 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-47K | 23 |
| R314 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-100K | 23 |
| R315 | $82 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-82K | 23 |
| R316 | $100 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-100K | 23 |
| R317 | $100 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | Nila | R12-100K | 23 |
| R318 | $10 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-10 | 23 |
| R319 | Not Used |  |  |  |  |  |  |
| R320 | $4.7 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | Eb | R1-4.76 | 23 |
| R321 | Not Used |  |  |  |  |  |  |
| R322 | 100 a | 10\%, 1/2W | Comp | 01121 | EB | RI-100 | 23 |
| R323 | $2.7 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12~2.7K | 23 |
| R324 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-100K | 23 |
| R325 | $47 \mathrm{k} \Omega$ | 10\%, 1/2 W | comp | 01121 | EB | R1-47K | 23 |
| R326 | $22 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-22K | 23 |
| R327 | $10 \mathrm{k} \Omega$ | 20\%, 2 W | WWVar | 71450 | 1NS 115 | RP50-10K | 23 |
| R328 | $91 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | NILA | R12-91K | 23 |
| R329 | $56 \Omega$ | 10 W |  | 91637 | HLM-10 | R138-56 | 23 |
| R330 | $2.7 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-2.7K | 23 |

POWER SUPPLY (cont'd)
RESISTORS (cont'd)

| $\begin{aligned} & \text { Circuit } \\ & \text { Desig. } \end{aligned}$ | Value | Rating | Type | Mfr. <br> Code | Mfr. Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R331 | $600 \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-600 | 22 |
| R332 | $1.8 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-1.8K | 22 |
| R333 | $1 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N1.1A | R12-1K | 22 |
| R334 | $2.7 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-2.7K | 22 |
| R335 | $1.8 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-1.8K | 22 |
| R336 | $2.73 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | Nila | R12-2.73K | 22 |
| R337 | 390 ת | 10\%, 1/2 W | Comp | 01121 | EB | R1-390 | 22 |
| R338 | $1 \mathrm{k} \Omega$ | 20, 2 W | WwVar | 71450 | 1NS 115 | RP50-1K | 22 |
| R339 | $1.4 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R1-1.4K | 22 |
| R340 | $2.2 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | R1-2.2K | 22 |
| R341 | $3.3 \mathrm{k} \Omega$ | 10\%, 1/2 W | Comp | 01121 | EB | RL -3.3K | 22 |
| R342 | $20 \mathrm{k} \Omega$ | 1\%, l/2 W | DCb | 00327 | N11A | R12-30K | 22 |
| R343 | $20 \mathrm{k} \Omega$ | 1\%, 1/2 W | DCb | 00327 | N11A | R12-20K | 22 |
| R344 | $33 \Omega$ | 10\%, 1 W | Comp | 01121 | GB | R2-33 | 20 |
| R345 | $4.7 \Omega$ | 10\%, 1/2 W | Comp | 011.21 | EB | R1-4.7 | 23 |

TRANSISTORS

| Circuit Desig. |  | $\begin{aligned} & \text { Mfr. } \\ & \text { Code } \\ & \hline \end{aligned}$ | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q301 | PNP | 02735 | 2NIL83A | TG-31 | 22 |
| Q302 | PNP | 02735 | 2N1183A | TG-31 | 22 |
| Q303 | NPN, Case TO-5 | 02734 | 40317 | TG-43 | 23 |
| Q304 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q305 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q306 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q307 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q308 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q309 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q310 | NPN, Case TO-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q311 | NPN, Case T0-5 | 02734 | 40317 | TG-43 | 23 |
| Q312 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q313 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q314 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q315 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 23 |
| Q316 | PNP | 01295 | 2N1381 | TG-8 | 22 |
| Q317 | PNP | 04713 | 2N1535 | TG-7 | 20 |
| Q318 | PNP | 01295 | 2N1381 | TG-8 | 22 |
| Q319 | PNP | 01295 | 2N1381 | TG-8 | 22 |
| Q320 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 22 |
| Q321 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 22 |
| Q322 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 22 |

REMOTE HEAD PARTS
(Refer to Schematic $21381 E$ for circuit designations).
Amplifier, $\mathrm{PC}-151, \mathrm{PC}-153, \mathrm{PC}-249$
CAPACITORS

| Circuit Desig. | Value | Rating | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *C101 | 150 pF | 500 V | Poly | 71590 | CPR-150J | C138-150P | - |
| *C102 | 6.5 pF | --- | --- | 80164 | --- | C31-5P \& C77-1.5P | , |
| *C103 | --- | --- | --- | 80164 | - | 13410A | - |
| C104 | 10 pF | 20 V | ETT | 05397 | K10.J20K | C80-10M | 26 |
| Cl 05 | 20 pF | --- | --- | 80164 | 215578 | 21557B | - |
| C106 | Not Used |  |  |  |  |  |  |
| C107 | 2.2 HF | 20 V | ETT | 05397 | K2R2J20K | C80-2.2M | 24 |
| Cl08 | 5 pF | 1000 V | CerD | 71590 | DD-050-10\% | C22-5P | 24 |
| C109 | 2.2 HF | 20 V | ETT | 05397 | K2R2J20K | C80-2.2M | 24 |
| C110 | Not Used |  |  |  |  |  |  |
| C111 | . $10 \mu \mathrm{~F}$ | 50 V | My | 84411 | 601PE | C41-.1M | 24 |
| C1.12 | $10 \mu \mathrm{~F}$ | 20 V | EtT | 05397 | K10.J20K | C80-10M | 24 |
| Cl13 | $2.2 \mu \mathrm{~F}$ | 20 V | ETT | 05397 | K2R2J20K | C80-2.2M | 24 |
| C114 | 5 pF | 1000 V | CerD | 71590 | [D-050-10\% | C22-5P | 24 |
| C115 | Not Used |  |  |  |  |  |  |
| C116 | 2.2 HF | 20 V | ETT | 05397 | K2R2J20K | C80-2.2M | 24 |
| C117 | . $1 . \mu \mathrm{F}$ | 50 V | My | 84411 | 601 PE | C41-. 1 M | 24 |
| Cl18 | $10 \mu \mathrm{~F}$ | 20 V | ETT | 05397 | K10J20K | C80-10M | 24 |
| Cl19 | . $02 \mu \mathrm{~F}$ | 1000 V | CerD | 56289 | 10ss-S20 | C22-.02M | 24 |
| C120 | . $02 \mu \mathrm{~F}$ | 1000 V | CerD | 56289 | 10ss-S20 | C22-.02M | 24 |
| C121 | Vibrating | Capacitor | --- | 80164 | -"- | VC-2 | - |
| C122 | . $001 \mu \mathrm{~F}$ | 1000 V | CerD | 72982 | $801000 \times 5 \mathrm{FO} 102 \mathrm{~K}$ | C22-.001M | - |
| C123 | . $001 \mu \mathrm{~F}$ | 1000 V | Cerd | 72982 | 801000X5F0102K | C22-.001M | - |
| C124 | 15-60pF | 500 V | CerD | 72982 | 538-011-P3PO-112R | C158-15/60P | - |
| C125 | 100 pF | 600 V | CerD | 72982 | ED-100 | C22-100P | - |
| C126 | $10 \mu \mathrm{~F}$ | 600 V | Cerd | 71590 | TCZ | C77-10M | - |
| C127 | 100 pF | 1000 V | Cerd | 71590 | DD-101-10\% | C22-100P | - |
| C128 | $0.1 \mu \mathrm{~F}$ | 50 V | My | 84411 | 601 PE | C41-. 1M | - |
| C129 | . $001 \mu \mathrm{~F}$ | 1000 V | CerD | 72982 | $801000 \times 5 \mathrm{~F} 0102 \mathrm{~K}$ | C22-.001M | - |
| C130 | Not Used |  |  |  |  |  |  |
| C131 | 1.5 pF | 600 V | Cert | 80164 | C123-1.5P | C123-1.5P | - |

* Nominal Value.

| Circuit Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D101 | Silicon | 01295 | 1N645 | RF-14 | 26 |
| D102 | Sil.icon | 01295 | 1N645 | RF-14 | 26 |
| D201 | Silicon | 73445 | 1N3182 | RF-31 | - |
| D202 | Silicon | 01295 | 1N914 | RF-28 | - |
| D203 | Silicon | 01295 | 1 N 91.4 | RF-28 | - |


| Circuit Desig. | Description | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $J 101$ | Connector, Receptacle (Mfg. No.57-40240) | 02660 | 5740240 | CS-196 | - |
| P401 | Connector, Plug, mate of J101 (Mfg. No. 57-30240) | 02660 | 5730240 | CS-195 | - |
| J102 | Connector, Plug, PC-153 | 80164 | --- | CS-197 | - |
| P102 | Connector, Pin, mate of J102 | 80164 | --- | CS-198 | - |
| $J 103$ | Test Jack, FEEDBACK | 80164 | --- | TJ-1 | 3 |
| J104 | Test Jack Connector Pin | 80164 | --- | CS-198 | - |
| J105 | Input Connector Contact Assembly | 80164 | --- | 20613A | 3 |
| --- | Input Cup, Adapter Assembly consisting of an adapter cap, (20569A) a contact cap (20568A) and a UHF connector (CS-64) | 80164 | --- | 21146B | - |
| -- | Dust cover | 80164 | --- | 20911A | - |
| J106 | Connector, Plug | 80164 | --- | CS-197 | - |
| P106 | Connector Pin, mate of J106 | 80164 | --- | CS-198 | - |
| J107 | Connector, Plug | 80164 | --- | CS-197 | - |
| P107 | Connector Pin, mate of J107 | 80164 | --- | CS-198 | - |
| J108 | Connector, S101 | 80164 | --- | CS-197 | - |
| P108 | Connector Pin, mate of J108 | 80164 | --- | CS-198 | - |
| J109 | Connector, S101 | 80164 | --- | CS-197 | - |
| P109 | Connector Pin, mate of Jl09 | 80164 | --- | CS-198 | - |
| S101 | Push Button Switch, ZERO CHECK (input head) | 80164 |  | SW-223 | 3 |
| --- | Knob Assembly, Zero Check | 80164 | --- | 16373A | 3 |
| S102 | Rotary Switch less components, SHUNT RESISTOR | 80164 | --* | SW-237 | 3 |
| --- | Rotary Switch with components, Shunt Resistor | 80164 | --- | 211438 | 3 |
| QA101 | Integrated Circuit | 12040 | LM201 | IC-2 | - |
| K101 | Solenoid Assembly | 80164 | --- | 21553B | - |
| K102 | Reed Relay | 27682 | GP1A650MW | RL-31 | - |
| L101 | Choke | 80164 | --* | $\mathrm{CH}-13$ | - |

RESISTORS

| Circuit Desig. | Value | Rating |  | Type | Mfr. Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R101 | 1 M | 1\%, 1/2 | W | MtF | 07716 | CEC | R113-1M | - |
| R102 | $10^{8}$ ת | 1\% |  | Comp | 03888 | HR 1000 | R144-10 ${ }^{8}$ | - |
| R103 | $10^{10}$ ת | $\cdots$ |  | GCb | 63060 | RX-1 | R20-10 ${ }^{10}$ | - |
| R104 | $10^{12} \Omega$ | --- |  | GCb | 63060 | RX-1 | R20-10 ${ }^{12}$ | - |
| R105 | 10 M \% | 10\%, 1/4 | W | Comp | 44655 | RC07 | R76-10M | - |
| R106 | 1 M $\Omega$ | 10\%, 1/4 |  | Comp | 44655 | RC07 | R76-1M | 24 |
| R107 | $10^{8}$ ת | 20\%, 1/2 | W | Comp | 75042 | GBT | R37-10 ${ }^{8}$ | 24 |
| R108 | $7.5 \mathrm{M} \Omega$ | 40\%, 0.3 | W | Cb | 71450 | SERIES 70 | RP71-7.5M | 24 |
| R109 | $10^{8} \Omega$ | 20\%, 1/2 | W | Comp | 75042 | GBT | R37-108 | 24 |
| R110 | $68.1 \mathrm{k} \Omega$ | 1\%, 1/8 | W | MtF | 07716 | CEA | R88-68.1K | 24 |
| R111 | $1.5 \mathrm{k} \Omega$ | 10\%, 1/4 |  | Comp | 44655 | RC07 | R76-1.5K | 24 |
| R112 | $47 \mathrm{k} \Omega$ | 10\%, 1/4 |  | Comp | 44655 | RC07 | R76-47K | 24 |
| R113 | $12 \mathrm{k} \Omega$ | 10\%, 1/4 |  | Comp | 01121 | CB | R76-12K | 24 |
| R114 | $5.6 \mathrm{k} \Omega$ | 10\%, 1/4 |  | Comp | 44655 | RC07 | R76-5.6K | 24 |
| R115 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 |  | Comp | 01121 | CB | R $76-68 \mathrm{~K}$ | 24 |

REMOTE HEAD (cont'd)
RESISTORS (cont'd)

| $\begin{aligned} & \text { Circuit } \\ & \text { Desig. } \end{aligned}$ | Value | Rating | Type | Mfr. Code | Mfr. Part No. | Keithley $\qquad$ | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R116 | $12 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R $76-12 \mathrm{~K}$ | 24 |
| R117 | $2.2 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-2.2K | 24 |
| R118 | $8.2 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-8.2K | 24 |
| $R 119$ | 100 k ת | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100K | 24 |
| R120 | $100 \mathrm{k} /$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100 | 24 |
| R121 | $12 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-12K | 24 |
| R122 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-68K | 24 |
| R123 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-68K | 24 |
| R124 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-68K | 24 |
| R125 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R $76-68 \mathrm{~K}$ | 24 |
| R126 | $10 \mathrm{M} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10M | 24 |
| R127 | $12 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R $76-12 \mathrm{~K}$ | 24 |
| R128 | $1 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-1K | 24 |
| R129 | $68 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-68K | 24 |
| R130 | $47 \mathrm{k} \Omega$ | 10\%, l/4 W | Comp | 44655 | RCO7 | R76-47K | 24 |
| R131 | $270 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-270K | 24 |
| R132 | $150 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-150K | 24 |
| R133 | $1.5 \mathrm{k} \Omega$ | 10\%, l/4 W | Comp | 44655 | KC07 | R76-1.5K | 24 |
| R134 | $8.2 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-8.2K | 24 |
| R135 | $100 \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100 | 24 |
| R136 | $4.7 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-4.7K | 24 |
| R137 | $18 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-18K | 24 |
| R138 | $18 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-18K | 24 |
| R139 | 390 ת | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-390 | 24 |
| R140 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10K | 24 |
| R141 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-10K | 24 |
| R142 | $4.7 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-4.7K | 24 |
| R143 | $100 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100K | 24 |
| R144 | $100 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100K | 24 |
| R145 | $22 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-22K | 24 |
| R146 | $180 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 01121 | CB | R76-180K | 24 |
| R147 | $100 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100K | 24 |
| R148 | $150 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-150K | 24 |
| R149 | 390 ת | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-390 | 24 |
| R150 | 100 k ת | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-100K | 24 |

TRANSISTORS

| $\begin{aligned} & \text { Circuit } \\ & \text { Desig. } \end{aligned}$ |  | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q101 | N-Channel Fet | 04713 | 2N4220 | TG-42 | 21 |
| Q102 | NPN, Case T0-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q103 | NPN, Case ro-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q104 | NPN, Case T0-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q105 | NPN, Case T0-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q106 | PNP, Case T0-92 | 04713 | 2N5087 | TG-61 | 21 |
| Q107 | N-Channel FET, Case $\mathrm{TO-92}$ | 04713 | MPF103 | TG-41 | 21 |
| Q108 | NPN, Case ro-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q109 | NPN, Case T0-92 | 04713 | 2N5089 | TG-62 | 21 |
| Q110 | PNP, Case T0-92 | 04713 | 2N5087 | TG-61 | 21 |
| Q111 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 21 |
| Q112 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 21 |

REMOTE HEAD (cont'd)
Oscillator, PC-247

## CAPACITORS

| Circuit Desig. | Value |  | Rating | Type | Mfr, <br> Code | Mfr. Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C501 | 10 | $\mu \mathrm{F}$ | 35 V | ETT | 05397 | K10E35 | C170-10M | 27 |
| C502 | 7-25 | pF | 350 V | Trimmer | 72982 | 538-011-93R | C89-7-25P | 27 |
| *C503 | 100 | pF | 200 V | Poly | 84171 | 2PJ-101G | C108-100P | 27 |
| C504 | 10 | pF | 500 V | Poly | 71590 | CPR-10J | C138-10p | 27 |
| C505 | 5 | pF | 200 V | Poly | 00686 | E1013-1 | C31-5P | 27 |
| C506 | 47 | pF | 500 V | Poly | 71590 | CPR-47J | C138-47P | 27 |
| C507 | 47 | pF | 1000 V | CerD | 71590 | DD-470-10\% | C22-47P | 27 |
| C508 | 1 | $\mu \mathrm{F}$ | 35 V | ETT | 05397 | K1E35 | C170-1M | 27 |
| *C509 | 100 | $\mu \mathrm{F}$ | 200 V | Poly | 84171 | 2PJ-101G | C108-100P | 27 |
| C510 | . 001 | $\mu \mathrm{F}$ | 1000V | CerD | 72982 | 801000×5F0102K | C22-.001M | 27 |
| C511 | 10 | $\mu \mathrm{F}$ | 35 V | ETT | 05397 | K10E35 | C170-10M | 27 |
| C512 | . 01 | $\mu \mathrm{F}$ | 1000 V | CerD | 56289 | 10SS-S10 | C22-.01M | 27 |
| C513 | 10 | $\mu \mathrm{F}$ | 35 V | ETT | 05397 | K10E35 | C170-10M | 27 |
| C514 | . 0047 |  | 1000 V | CerD | 56289 | 10SS-D47 | C22-.0047M | 27 |
| C515 | . 01 | $\mu \mathrm{F}$ | 1000 V | Cerd | 56289 | 10ss-S10 | C22-.01M | 27 |
| C516 | 10 | PF | 1000 V | CerD | 71590 | DD-100-10\% | C22-10P | 27 |
| C517 | . 01 | ${ }^{\mu} \mathrm{F}$ | 200 V | My | 13050 | SM1A | C47-.01M | 27 |
| C518 | 100 | PF | 1000V | CerD | 71590 | DD-101-10\% | C22-100P | 27 |
| C519 | . 047 | $\mu \mathrm{F}$ | 200 V | My | 13050 | SM1A | C47-.047M | 27 |
| C520 | 10 | $\mu \mathrm{F}$ | 35 V | ETT | 05397 | K10E35 | C170-10M | 27 |

## DIODES

| Circuit Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D501 | Silicon | 01295 | 1N914 | RF-28 | 27 |
| D502 | Silicon | 01295 | 1N914 | RF-28 | 27 |
| D503 | Silicon | 01295 | 1N914 | RF-28 | 27 |
| D504 | Silicon | 01295 | 1N914 | RF-28 | 27 |

INTEGRATED CIRCUITS

| Circuit <br> Desig. | Type | Mfr. <br> Code | Mfr. <br> Part | Kefthley <br> Part No. | Fig. <br> Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- |
| QA501 | Integrated Circuit | 07263 | U5B770939X | IC-1 | 27 |
| QA502 | Integrated Circuit | 07263 | U5B770939X | IC-1 | 27 |
| QA503 | Integrated Circuit | 07263 | U5B770939X | IC-1 | 27 |

RESISTORS

| Circuit <br> Desig. | Value. | Ratingg | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R501 | $10 \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10 | 27 |
| R502 | $1 \mathrm{M} \Omega$ | 1\%, 1/2 W | MtF | 07716 | CEC | R94-1M | 27 |
| R503 | 32.4 K ת | 1\%, 1/8 W | MtF | 07716 | CEA | R88-475 | 27 |
| R504 | $32.4 \mathrm{~K} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-32.4K | 27 |
| R505 | $9.31 \mathrm{~K} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-9.31K | 27 |

*Nominal Value, Selected during calibration.

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REMOTE HEAD (cont'd)
    OSCILLATOR
RESISTORS (cont'd)
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| Circuit Desig. | Value | Rating | Type | Mfr. <br> Code | $\begin{aligned} & \text { Mfr. } \\ & \text { Part No. } \end{aligned}$ | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R506 | $1 \mathrm{k} \Omega$ | 20\%, . 75 W | Cermet | 73138 | 77 PR | RP64-1K | 27 |
| *R507 | $301 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-301K | 27 |
| R508 | $10 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-10K | 27 |
| R509 | 10 ת | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10 | 27 |
| R510 | $1 \mathrm{M} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-1M | 27 |
| R511 | $5.62 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-5.62K | 27 |
| R512 | $1.5 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-1.5K | 27 |
| R513 | $442 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-442K | 27 |
| R514 | $22.1 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-22.1K | 27 |
| R515 | $2.21 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-2.21K | 27 |
| RS16 | $22 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-22K | 27 |
| R517 | $10 \mathrm{k} \Omega$ | 20\%, 2 W | --- | 10582 | 115-117 | RP58-10K | 27 |
| R518 | $402 \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-402 | 27 |
| R519 | $442 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-442K | 27 |
| R520 | $14.7 \mathrm{k} \Omega$ | $1 \%, 1 / 8 \mathrm{~W}$ | MtF | 07716 | CEA | R88-14.7K | 27 |
| R521 | $10 \mathrm{k} \Omega$ | 20\%, 2 W | --- | 10582 | 115-117 | RP58-10K | 27 |
| R522 | $10 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-10K | 27 |
| R523 | $100 \mathrm{k} \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-100K | 27 |
| R524 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10K | 27 |
| R525 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10K | 27 |
| R526 | $49.9 \Omega$ | 1\%, 1/8 W | MtF | 07716 | CEA | R88-49.9 | 27 |
| R527 | $1 \mathrm{k} \Omega$ | $1 \%, 1 / 8 \mathrm{~W}$ | MtF | 07716 | CEA | R88-1K | 27 |
| R528 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10K | 27 |
| R529 | 10 ת | 10\%, 1/4 W | Comp | 44655 | $\mathrm{RCO7}$ | R76-10 | 27 |
| R530 | $10 \mathrm{k} \Omega$ | 10\%, 1/4 W | Comp | 44655 | RC07 | R76-10K | 27 |

TRANSFORMERS

| Circuit Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T501 | --- | 80164 | TR-132 | TR-132 | 27 |
| T502 | --- | 80164 | TR-132 | TR-132 | 27 |

TRANSISTORS

| Circuit Desig. | Type | Mir. <br> Code | Mfr. $\qquad$ | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q501 | Sliscon, NPN, Case TO-92 | 04713 | 2N5089 | TG-62 | 27 |
| Q502 | Silicon, NPN, Case TO-92 | 04713 | 2N5089 | TG-62 | 27 |
| Q503 | N -Channel FET, Case TO-92 | 04713 | MPF103 | TG-41 | 27 |
| Q504 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 27 |
| Q505 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 27 |
| Q506 | PNP | 01295 | 2N1381 | TG-8 | 27 |
| Q507 | PNP | 01295 | 2N1381 | TG-8 | 27 |

*Nominal Value, Selected during calibration.

## CODE-TO-NAME LIST

CODE TO NAME List of Suggested Manufacturers.
Reference: Federal Supply Code for Manufacturers, Cataloging Handbook H4-2.

| 00656 | Aerovox Corp. <br> 740 Belleville Ave. <br> New Bedford, Mass. 02741 | 07137 | $\begin{aligned} & \text { Transistor Electronics Corp. } \\ & \text { Hwy. } 169 \text { - Co. Rd. } 18 \\ & \text { Minneapolis, Minn. } 55424 \end{aligned}$ | 14659 | Sprague Electric Co. P.O. Box 1509 <br> Visalia, Calif. 93278 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00686 | Film Capacitora, Inc. 100 Eighth St. Passaic, N.J. | 07263 | Pairchild Camera \& Inst. Corp. 313 Frontage Road Mountain View, Calif. | 15238 | ITT Semiconductors Div. of ITT Corp. Lawrence, Mass. 01841 |
| 01121 | Allen-Bradley Corp. 1201 South 2nd St. Milwaukee, Wisc. 53204 | 07716 | IRC, Inc. <br> 2850 Mt . Pleasant <br> Burlington, Lowa 52601 | 15909 | Daven Div, of T.A. Edison Ind. McGraw Ediaon Co. Livingston, N.J. |
| 01295 | $\begin{aligned} & \text { Texas Instrumenta, Inc. } \\ & \text { Semiconductor-Components Div. } \\ & \text { Dallas, Texas } 75231 \end{aligned}$ | 08811 | GL Electronics Div. of GL Industries, Inc. Westville, N.J. 08093 | 16170 | Teledyne Systems Co. Communications Div. Los Angeles, Calif. 90066 |
| 01686 | RCL Electronics, Inc. 195 McGregor St. Manchester, N.H. 03102 | 09052 | Gulton Induatries, Inc. Alkaline Battery Div. Metuchen, N.J. | 17554 | Components, Inc. Smith St. <br> Biddeford, Ma. 04005 |
| 02101 | Varo Inc, Electrokinetics Div. <br> Santa Barbara, Ca1if. 93102 | 09823 | Burgess Battery Co. Div, of Servel Inc. Freeport, Ill. | 23020 | General Reed Co. 174 Main St. <br> Metuchen, N.J. 08840 |
| 02660 | Amphenol Corp. <br> 2801 South 25th Ave. <br> Broadview, I11. 60153 | 09922 | Burndy Corp. <br> Richards Ave. <br> Norwalk, Conn, 06852 | 24655 | General Radio Co. 22 Baker Ave. West Concord, Mass. 01781 |
| 02734 | ```Radio Corp, of America Defense Electronic Producta Camden, N.J.``` | 10582 | CTS of Asheville Inc. Mills Gap Road Skyland, N.C. | 27682 | Hathaway Instrumente, Inc. <br> 5800 E. Jewell Ave. <br> Denvar, Colorado 80222 |
| 02735 | Radio Corp, of America Receiving Tube Div. Somerville, N.J. | 11502 | IRC Inc. Greenway Road Boone, N.C. 28607 | 28520 | Hayman Mfg. Co. 147 N. Michigan Ave. Renilworth, N.J. |
| 02777 | Hopkins Engineering Co. 12900 Poothill Bivd. <br> San Eernando, Calif. 91342 | 11837 | Electro Scientific Indus., Inc. 13645 NW Sciance Park Dr. Portland, Or. 97229 | 29309 | Richey Electronics Inc. 1307 Bickerson Rd. Nashville, Tenn. 37213 |
| 02985 | Tepro Electric Corp. 5 St. Paul St. Rochester, N.Y. 14604 | 12040 | National Semiconductor Corp. Commerce Drive <br> Danbury, Conn. 06813 | 35529 | Leads and Northrup 4901 Stenton Ave. Philadelphia, Pa. 19144 |
| 03508 | General Electric Co. Semiconductor Products Dept. Syracuse, N.Y. 13201 | 12065 | Transitron Electronic Corp. 144 Addison St. <br> East Boston, Mass. | 37942 | Mallory, P. R. and Co., Inc. 3029 E . Washington St. Indianapolis, Ind. 46206 |
| 04009 | Arrow-Hart \& Hegeman Electric Co. 103 Hawthorne St. Hartford, Conn. 06106 | 12697 | Claroatat Mfg. Co., Inc. Lower Washington St. Dover, N.H. 03820 | 44655 | Ohmite Mfg. Co. 3601 Howard St. Skokie, I11. 60076 |
| 04713 | Motorola Semiconductor Prod. Inc. 5005 E. McDowell Rd. <br> Phoenix, Ariz. 85008 | 12954 | Dickson Electronics Corp. 302 S. Wells Fargo Ave. Scottsdale, Ariz. | 53201 | Sangamo zlectric Co. 1301 North 11th Springfiald, Ill. 62705 |
| 05079 | ```Tansistor Electronics, Inc. 1000 West Road Bennington, Vt. 05201``` | 13050 | Potter Co. <br> Highway 51 N . <br> Wesson, Miss. 39191 | 54294 | ```Shallcross Mfg. Co. 24 Preston St. Selma, N.C.``` |
| 05397 | Union Carbide Corp. Electronics Div. New York, N.Y. 10017 | 13327 | Solftron Devices, Inc. 256 Oak Tree Road Tappan, N.Y. 10983 | 56289 | Sprague Electric Co. North Adame, Masaachusetts |
| 06751 | Components, Inc. Arizona Div. Phoenix, Ariz. 85019 | 13934 | Midwec Corp. <br> 602 Main <br> Oshkosh, Nebr. 69154 | 58474 | Superior Electric Co., The 383 Middle St. <br> Bristol, Conn. 06012 |
| 06980 | Varian Assoc. EIMAC Div. 301 Industrial Way San Carlos, Calif. 94070 | 14655 | ```Cornell-Dubilier Rlectric Corp. 50 Paris Street Newark, N.J.``` | 61637 | Union Carbide Corp, 270 Park Ave. <br> New York, N.Y. 10017 |


| 63060 | Victoreen Instrument Co. 5806 Hough Ave. <br> Cleveland, Ohio 44103 | 75042 | IRC Inc. <br> 401 North Broad st. <br> Philadelphia, Pa, 19108 | 86684 | Radio Corp. of Americe Electronic Components \& Devices Harrison, N.J. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 70309 | Allied Control Co., Inc. 2 East End Ave. New York, N.Y. | 75915 | Littlefuse, Inc. 800 E. Northwest Hwy. Des Plaines, I11. 60016 | 87216 | Philco Corp. <br> Lansdale Div., Church Rd. Lansdale, Pa. 19446 |
| 70903 | Belden Mfg. Co. 415 So. Kilpatrick Chicago, Ill. 60644 | 76055 | Mallory Controls, Div. of Mallory P. R. \& Co., Inc. Frankfort, Ind. | 90201 | Mallory Capacitor 3029 East Washington Indianapolis, Ind. 46206 |
| 71002 | Birnbach Radio Co., Inc. <br> 147 Hudson St. <br> New York, N.Y. | 76493 | Miller, J. W. Co. <br> 5915 S . Main St. <br> Los Angeles, Calif. 90003 | 90303 | Mallory Battery Co. Tarrytown, New York |
| 71279 | Cambridge Thermionic Corp. 430 Concord Avenue Cambridge, Mass. | 76545 | Mueller Electric Co. 1583 E. 31st St. Cleveland, Ohio 44114 | 91637 | Dale Electronics, Inc. P.O. Box 609 Columbus, Nebr, 68601 |
| 71400 | Bussmann Mfg. <br> Div. of McGraw-Edison Co. <br> St. Louis, Mo. | 77764 | Resistance Products Co. 914 S. 13th St. <br> Harrisburgh, Pa. 17104 | 91662 | Elco Corp. Willow Grove, Pennsylvania |
| 71450 | CTS Corp. <br> 1142 W. Beardslay Ave. <br> Elkhart, Ind. | 79727 | Continental-Wirt Electronics Corp. Philadelphia, Pa, | 91737 | Gremar Mfg. Co., Inc. 7 North Ave. Wakefield, Mass. |
| 71468 | ITT Cannon Electric, Inc. 3208 Humbolt St. <br> Los Angeles, Calif. 90031 | 80164 | Keithley Instruments, Inc. 28775 Aurora Road Cleveland, Ohio 44139 | 91802 | Industrial Devices Inc. 982 River Rd. <br> Edgewater, N.J. 07020 |
| 71590 | Centralab Div. of Globe-Union, Inc. Milwaukee, Wisc. 53212 | 80294 | Bourns, Inc. 6135 Magnolia Ave. Riverside, Calif. 92506 | 91929 | Honeywell Inc. <br> Micro Switch Div. <br> Freeport, Ill. 61032 |
| 71785 | Cinch Mfg. Co, and Howard B. Jones Div. Chicago, I11. 60624 | 81073 | Grayhil1, Inc. 561 Hillgrove Ave. La Grange, I11. 60525 | 93332 | Sylvania Electric Products, In Semiconductor Products Div. Woburn, Mass. |
| 72619 | Dialight Corp. <br> 60 Stewart Ave. <br> Brooklyn, N.Y. 11237 | 81483 | International Rectifier Corp. 1523 East Grand Ave. <br> El Segundo, Calif. | 93656 | Electric Cord Co. 1275 Bloomfield Ave. Caldwell, N.J. |
| 72653 | G-C Electronics Co. 400 S . Wyman Rockford, Ill. 61101 | 82389 | Switcheraft, Inc. 5527 N . Elston Ave. Chicago, I11. 60630 | 94144 | Raytheon Co., Industrial Operation Components Div. Quincy, Mass. |
| 72699 | General Instrument Corp. Capacitor Division Newark, N.J. 07104 | 83125 | General Instrument Corp. Capacitor Division Darlington, S.C. 29532 | 94154 | ```Tung-Sol Electric, Inc. Newark, New Jersey``` |
| 72982 | Erie Technological Prods Inc. 644 W. 12th St. <br> Grie, Pa. 16512 | 83330 | Smith, Herman H., Inc. 812 Snediker Ave. Broaklyn, N.Y. 11207 | 94310 | Tru-Ohm Producta Memcor Components Div. Huntington, Ind, 46750 |
| 73138 | Becknan Instruments, Inc. Helipot Division <br> Fullerton, Calif. 92634 | 83594 | Burroughs Corp. <br> Electronic Components Div. <br> Plainfield, N.J. 07061 | 94696 | Magnecraft Electric Co, 5579 North Lynch Chicago, 111. |
| 73445 | Amperex Electronic Co, Div, of North American Philips Co., Inc. Hickaville, N.Y. | 83701 | Electronic Devices, Inc. <br> Brooklyn, <br> New York | 95348 | Gordos Corp. 250 Glenwood Ave. Bloomfield, N.J. 07003 |
| 73690 | Elco Resistor Co. 1158 Broadway New York, N.Y. | 84171 | Arco Electronics, Inc. Compunity Drive Great Neck, N.Y. 11022 | 95712 | Dage Electric Co., Inc. Hurricane Road Franklin, Ind. |
| 74276 | Signalite Inc. 1933 Heck Ave. Neptune, N.J. 07753 | 84411 | TRW Capacitor Div. 112 W. First St. Ogallala, Nebr. | 97933 | Raytheon Co. Components Div, Semiconductor Operation Mountain View, Calif. |
| 74970 | Johnson, E. F., Co. 297 Tenth Ave. S.W. Waseca, Minn. 56093 | 84970 | Sarkes Tarzian, Inc. E. Hillside Dr. Bloomington, Ind. | 99120 | Plastic Capacitors, Inc. 2620 N. Clybourn Ave. Chicago, Ill. |






[^0]:    *Matched pair, order TG-40 for pair.

