# MODEL 150 <br> and <br> MODEL 150 R <br> DC MICRO VOLT.AMMETER <br> INSTRUCTION MANUAL. 

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The Model 150 Micro Volt-Ammeter is a stable, versatile instrument for moasuring extremely low level DC signals. It functions as a voltmeter from one microvolt to one volt full scale, and as an ammeter from one milliampere to one hundred micro-microanperes full scale. It also opcrates as a DC amplifier with gains up to ten million for driving recorders.

The very low notse level of the Model 150, together with its lone term stability make it ideal for many measurements roquiring oxtreme power sensitivity.

Typical applications include moasuring the output from strain gaces, thermopiles, thermocouples, bolometers, phototubes, ionization chamburs, scintillation countors, and barrier layer colls. Othor applications are found in cell studies, measurement of electrochemical potentials, electrolytic corrosion studies, molecular weight analysis and Hall offect studies.

In addition to its use as a direct indicator of minute potentials and currents, the Modol 150 may also be usod as a null detector in Wheatstone or Mueller bridges, or with an extornal vol.tage source ab a meg-mogohmmeter.

An important feature of the instrument is zero suppression up to 100 times full scale, in place of the usual more limited meter zero. This permits measurements of small signals in the presence of large thormal EMF's or other masking DC signals.

## VOLIMETEIR SFECIFICATIONG

RANGES: 13 overlapping ranges in $1 x$ and $3 x$ steps from 1 - microvolt to 1 volt full scale on a zero-center meter.

ZERO STABILITY: After a one hour warm-up within +0.1 microvolt $\pm 2 \times 10^{-5} \mathrm{R}$ microvolts per day, where R is the source resistance in ohms.

NOISE: Vith the inout shorted, less than 0.03 microvolt peak to peak ( 0.006 microvolt RMS). At various source impedences the noise is given $\mathrm{ky} \mathrm{E}=6.5 \times 10^{-4}$ ( $\mathrm{R}+$ 2000) $\frac{1}{2}$ microvolts peak-to-peak since the ohmic input resistance is added to $R$, the source resistance.

ACCURACY: $2 \%$ of full scale on all ranges.
INPUT AND SOURCE RESISTANCE: As tabulated below unless resistora shunting the input are requested, in which case the input resistance is look on the microvolt ranges and 1 megohm on the millivolt ranges. The maximum source resibtance specifications on the 1 and 3 microvolt ianges hold with or without shunting input resistance.

RANGE:

Input Resistance Greater than

1 megohm
3 mogohms
10 megohms
30 megohms
90 megohms

Maximum Source Resistance
1 microvolt
3 microvolts
10 microvolts
30 microvolts
100 microvolts
and above

RPSPONSE SPEDD: (10 to $90 \%$ of full scalc.). With maximum specified source resistance, less than one second on all ranges excopt the 1 microvolt range whore it is two seconds. With source resistances less than $10 \%$ of maximum source resistance, response is within 0.5 second on all ranges, except the 1 microvolt range where it is within 1 second.

VOLTAGR ZFRO SUPPRFSS: Rancos, Oft, plin or minus 10,100 , 1000 and 10,000 microvolta; and 0.1, 1.0, $10.0,100.0$ millitvolts corrospondine to tho MICROVOLTS and MILLIVOLIS positions on tho function switch. Tho accuracy of the aupreasion ranees is upproximately $20 \%$ and the stability i.s such that 100 times full scale may be suppressed.

## AMMETER SFECIFICATIONS

RANGES: 15 overlapping ranges in $1 x$ and $3 x$ steps frou $10^{-10}$ to $10^{-3}$ ampere full scale on a zero center meter.

STABIIITY: After one hour warm-up, within plus or minus $2 x$ 10-11 ampere per day.

NOISE: Less than $2 \times 10-12$ ampere peak to peak.
ACCURACY: Plus or minus $3 \%$ of full scalo on all rangos.
VOLTAGE DROP: 100 microvolts on the millimicroampere ranges, I millivolt on the microampere ranges.

INPUT RESISTANCE: Equal to $1 \times 10^{-4}$ divided by current range on microamperes. (Input resistance on the 10-3 range is one ohm, rising to one megohm on the $10^{-10}$ ampere range).

RESFONSE SPEED: "One second except on the $10^{-10}$ range where it is two seconds.

CURRENT ZERO SUPPRESS: A maximum of 100 times full scale zero suppression on any range. Accuracy and stability are tho same as for voltage zerc suppress.

## GENERAL SFECIFICATIONS

RECORDER OUTPUT: Plus or minus 10 volts at five milliamperes for full-scale deflection on any range.

OUTPUT IMPEDANCE: Leas than 10 ohms below 1 cps .
60 CPS REJECTION: Greater than 50:1.
INPUT ISOLATTON: Negative terminal may be grounded or floating up to plus or minus 400 volts with respect to the case. A link is provided for grounding the negativo terminal to the case.

POWER REQUIREMENTS: $117 / 230$ volts, 50 watts, 60 cps only. 50 cps models on special order.

## A. OPMRATHIGG CONTROI.S

The controls of the Model 150 are simple and conveniently placed. Their functions are as follows:

ON-OFF switch is located to the right of the panel meter.

FUNCTION switch selects the function which is to be uscd; millivolts, microvolts, microamperes o: millimicroamperes.

RANGE switch selects the full scale multiplier of the function selected by the FUNCHION switch. Note that the 0.3 and 0.1 positions are to be used in current moasurement only.

ZERO SUPPRESS controls consist of the ZERO RANGS switch which selects the course range of supprossing voltage in discreet steps and the ZERO SEP potentiometer which gives continuously variable fine control including settings through zero.
B. PRELIMINARY SET-UP

Connect the instrument to the power Iine. Unless otherviso marked the unit may be used on 117 volt, 60 cps line. To convert to 220 -volt operation, refer to the MAINTENANCE soction. A three-wire line cord is furnished, which grounds the cabinet. If a three-wire recoptacle is not available, use the two-pin adapter furnished, and ground the third lead to an external ground.

Set controls as follows:
Function: Millivolts
Range: 1000
Zero Suppress: OFF
Input: Short the input loads together.

1. Source Resistance - In SECTION II - SPECIFICATIONS under INPUL AID SOUTCE RESISTANCE, the naximum source rosistance for use with each voltape ronce is spociffied. Reasonable oneration is possjble with source resistances up to ten times groater than those suecified, however the measurement will suifer from a consicerable docrease in speed of response, and moasuring accuracy. If the instrumont is left completely open-circuited, the meter will zenorally drift off acale on any voltage range. On current ranges this dues not happen becauso of the input shunting resistors.
2. Shiclding - Since tho instrument operates with a modulato: frequency of 120 cps , its is not genorally sensitive to 60 cos pickup unloss it is largo onouch to overload the amplifier. Tho pickup incy be a source of difficulty when using the amplifier with high imperiances on the more sensitive voltage ranges and on the tho or three most sensitive current ranges. In these cases it is desirable to shiold the leads and the source as completely as possible. In soins cases a simple low-pass filter at the input to eliminate frecuercies of about $l$ cps and above will be helpriul. No use is made of an input filter in this instrument since eny input serios irpedance due to the filter will increase the input noise and the thermal drift. When operating above ground, the case of the instrument must be crounded.
3. Thermal EMF - Extrome procautions have been taken in the input circuit to minimize thermal EMF's so that the residual FMF is less than 0.6 microvolt. The material used in the imput circuit is pure copper. Any other metal will generate a thermocouple potential. Load solder is particularly troublesome. Whero thormal TMF's aro a problem, soldering should be done with tho cadmium-tin solder sunplied with the instrument.
4. Input No1se: The noiso at the input is a function of input resistance and is approximately given by

$$
E=1.29 \times 10^{-10}(\mathrm{R}+2000) \frac{1}{2}
$$

whero $E$ is the $R M S$ noise, and $R$ is the source resistance. It is assumed that the bandwidth of the irstrument $1 s$ about 1 cps and the temperature is $80^{\circ} \mathrm{F}$. If noiso is observed, calculate the theoretical noise and compare results. Also bear in mind that only wire-wound resistors approach the ideal resistor. However, if Evaroha or manganin resistors are used, a considerable thermal 玉MF of the resistor material against copper will bo obsorved.
5. Checking the Zero Point - At low levels, spurious EMF's may bo generated simply by contact betwoen the input leads and the terminel.s under test. If possible, always leave tho instrument connected and adjust the zero after establiching a zero rorerence in the apparctus undor test. For example, in bridce measurements, disconnect tho bridge exciting voltage; or with a phototube, shield the tube irom licht.

## D. MFASURING VOHTACR

1. Diroct Voltace Moamuromonta - Place the FUNC'ION switch at MILIIVOLIS or MICiOVOLIS as nocessary for tho moasuroment to bo taken. Thon turn tho RANGE switch to more sensitive ranges until. the metor gives a usable doflection.
2. Moasuring Voltage Variations - Set tho FUNCTION switch and RAIGS switch to obtain the best deflection ar the meter. Use the ZERO SUPPIRSS controls as doscribed in $B$ to increase the sensitivity of tho metor. Then small changes in a relativoly large stendy sienal may be displayed with a large scale deflection.
3. Measuring Difforential Voltingos - Then measusenents are to bo made in a circuit where the LOW connoction $1 s$ ebove cround potontial, remove the DISCONNECT LINK from one of its posts. Ihis disconnects the instrumont circuit ground from chassis ground. DO NOT attempt to make such measurements where the low side of the circuit being measured is more than 400 volta abcve external ground potential.

If a recorder is being used with the instrument in this arrangenent, the recorder ground must not bo connected to the output ground of the ingtrument since the low side of the output would no longor be erounded.
F. MEASURING CURRENT

Direct Current Reading - Turn the FUNCIION SWITCH to MICROAIPS or MILLIMICROAMPS, and the RANGR SWITCH to 1000. Connect the instrument to the current source and sot the RANGF SWITCH to the range which gives the best deflection of the moter.

Measuring Current Variations - Proceed as above for airect current readings, and then use the ZERO SUPPRESS and ZERO SET as described under $B$.
F. OTHER APPLICATIONS

1. Null Indicator - The Model 150 makes an extremely sensitive null indicator which may be used in a Wheatstone or Mueller Bridge.

In a Wheatstone Bridge, the Model 150 is connected between the two resistor arms. With the FUNCRION SWITCH on MICROAMPS, and the RANGE SWITCH on 1000, the bridgo can be adjusted to give a zero reading on the meter. The instrument can then be set on more sensitive ranges for finor adjustrente of the bridge.*
2. Megohmeter - The Model 150 may be used to measure resistancos, utilizing an external voltage source and measuring the current which flows in the unknown.
*If the bridge is arranged so that one terminal of tho dotector is grounded, the Model 150 may be used as describod in E.l. If the detector must be used floating, remove the DISCONNECT LINK at the rear and observe the same precautions as in D.3.

Tho Model 150 is bacically a narrow-bend chopner amplifier employine nogativo foodback to stabilize tho gain and increaso the input impodance.

## A. Input Circuit

Zoro Stability: The effect of thermal EMF's goneretod. in the input circuitry is reduced to nearly the vanishing point by the use of only copper or silver materials in the input circuit. All solder joints are made with a low thermal cadmium-tin solder. the chopper and chopper transformer employ copper leads. All switching in the input circuit is accomplished with a solid silver swi.tch. Criticel resist,ors in the input circuit are wound of copper wire. The input connector has solid copper spring-loaded contacts.

The input voltage is applied to the moving arm of a 120 ops mechanical chopper. The feedback voltage is connected to the primary center tan of the input transformer. Thus, the difference voltage is applied first across ono half of the primary end then, with phase reversal, to the other half. This full wave error signal is stepped up 16 to 1 by the input transformer and applied to the grid or V1, a 6084 lownoiso pentode.

## B. AC Amplifier

In parallel with the plate load resiator of V1 is a relatively high Q, 120 cps resonant circuit which narrows tho bandwidth and reduces spurious signals.

V2 and V3, EF86 pentodes, further amplify the chopped error signel. which is then demodulated synchronously by germanium diodes D1 and D2.

To obtain the 120 cps demodulator driving sigmal, use is made of the ripple frequency from a bridge rectifier circuit operating from the line voltage. The ripple is connected to the primary of the demodulator driver transformer.
C. DC Amplifier

The demodulated signal is applied to the grid of V4. V4, V5, and Vo form the de amplifier and output cathode follower which add further forward gain to the system and supply output porer. Feedback around V4, V5 and V6 multiplies the effective cepacitance of demodulator filter capacitor Clil by about 1000. This yields the large equivalent capacitance necessary to smooth the demodulated error signel. Because of the reedback, spurious noise in the dc stages outside the pass band of tho whole amplifier are effectively degenerated.
D. Zero Suppression

A low-current $\pm 10$ volt supply is derived from the main de supplies using 20 -volt zener diodes. Potentiometer R174 may be set at any voltage from -10 to +10 volts; this voltage being applied through appropriate dropping resistors to the feedback point to achieve zero suppression. The potentiomoter is the front panel control marked ZERO SEI, while switch SW3, which determines the portion fed back, is labeled ZERO RANGE.

## E. Other Controls

Three controls are set at the factory and should requiro only infroquent attention by the user.

Rll 8 is an intornal control marked DC AMP BAJ. It is used to zero the DC amplifier, i.e., to set the output voltage to zero when the domodulator output is zero. This is not very critical since an unbalance will simply be fed back to the input to produce a small orror signal to correct itsolf. Rla7 is marked CAL. This is the variable portion of the meter multiplier resistance to allow for moter-to-moter sensitivity differences.

R177, marked CURRENT BALANCE, may be set at some vol.tace which will cause a current to flow through R175 to the chopper arm. This current is used to compensato for a small genorated "choppor current" which would otherwise flow in the input circuit. This "chopper current" differs from chopper to chopper but is fairly stable for long periods of time. Its effect on any current range could be removed with the ZERO SUPPRESS controls, but the Current Balanco inothod used here gives an effective zero input current for all ranges.
F. Power Supply

A standard half-wave rectifier followed by an R-C filter is used to supply unregulated $B+$ and $B$ - to the output cathode follower.

The unregulated $B$ - is regulated to -150 volts in $V 7, O A 2$, and is used for the negative returns for the de amplifier.

Unregulated $\mathrm{B}^{+}$is fed to the plate of $\mathrm{V} 8,12 \mathrm{~B} 4 \mathrm{~A}$, the series tube in a 225 -volt electronic regulator. The output voltage from this regulator is divided by R510 and R5ll and compared to reference tubo V9, a 5651. The difference aignal is amplified by cascode amplifier Vlo, a l2AX7, and applied to the grid-catnode circuit of the series tube. This regulated 225 volts supplies $B+$ directly to the de amplifier, through a decoupling filter ( R 176 , Cllo) to the second ana third ac amplifier stages, and through another decoupling filter (RI03, Cl04) to the first ac amplifier stage.

Regulated $B+a n d B-a l s o$ supply currents to the 10 volt zener diodes which are used for zero suppression. This gives two-stage regulation for these very critical voltages.

The first two ac amplifier filaments and the first dc amplifier filaments are driven by a bridage-rectified $\sigma$-volt d.c. supply. The R-C filler sections R512, C507, R5l3, C508, insure low ripple.

Except for occasional tube or chopper replacement, very little maintenance is roquired by the Models 150 and 150 R. Components are operated. well below rating and solid-stato devices are employed where possible to achieve lone, trouble-free service.

Certain portions of the input circuit are wired using copper wire and special cadmium-tin solder. These special joints are painted red. If, for any reason, these joints must be unsoldered or re-solderoc, USE ONLY CADMIUM-TIN SOLDER AND A COPPER-TIPPED SOLDERING IRUN WFICH HAS NEVER BEEN USED WITH ORDTNARY LEAD-TIN SOLDER. A small spool of cadmium-tin solder is supplied with each instrument.

What may seem to be circuit fallure in the Micro Volt-Ammeter is cuite often found to be an unusual condition in the entire test set-up. Therefore; before trouble-shooting the instrument, chock to see whethor it operates corroctly with:

1. All other circuitry disconnected.
2. Input shorted (with copper leads).
3. power line voltage and frequency correct.

If the difficulty persists, the following systematic procedure may be employed to determino the fault.

TROUBLE-SHOOTING
Reforence is made to the Schematic Diagram, DN 121.88-D, and the VoltageResistance Diagram enclosed at the rear of tho manual.

To bogin trouble-shooting, short the input terminals, strap chassis ground to LO with the link provided, and switch ZERO RANCE to CFF. A Zero orfset of a few tenths of a microvolt is normal. On curront functions with the input terminals open but shielded, it should be possible to set zero current with the CURRENT EALANCE control at the rear of tho inetrument.

EXCESSIVE OUTPUT NOISE (INPUT TERMINALS SHORTED)
Short the input grid of the de amplifier, pin 7 of V4, to ground. If this stops the noise, it is being generated in the ac amplifier. Unfortunately, because of the very low sienal levels involved, noise in the ac amplifior is difficult to trace by other than the substitution method. Most logical noise sourcos are Vl. or the chopper. To replace tho choppar, unplug the cap at the top, and unscrew the three thumb-screw nuts which clanp the chopper leads. Unscrew the two choppar mounting scrows and lift out the chopper. When inserting the new chonper, make sure that the chopper leads are pressed against the coppor termirals and that the insulating washers oro between tho leads and the thumb-screw nuts. Observe color-coding on the leads.

If the noise persigts aftor ahorting the dc amplifier input, the noise is buing goncrated in the de ampliffor or power supply. A stace-bystafe search should reveal the source.

OUTPUT NOT ZWRO (INPUT TWRMLNALS SHORTED)
Be sure that ZERO RANGE is set to OFF. Short the dc amplifier inpui erid, pin"? of VIt, to ground. Use the DC AMP BAL Control to sot the output to zero. If this cannot be done, the dc amplifier or power supply are at fault. If it can be sot to zero, the trouble may be in the ac amplifier or demodulator circuit.
a. Power Supply - $\mathrm{B}^{+}$should be about +225 on pin 1 of $V \delta$, and $B-$ should be -150 on pins 2,4 or 7 of $V 7$. If $V 7$ is not firing, correct the fault in the unregulated B-. If te25 is not present, check for unregulated $B+$ (about 340 volts) at the plate pin 9 of v8. If the unregulated $B+i s$ all right, check the tube pin voltages of $V 8$, V9, and V10 to locate the faulty tube or part. . .
b. AC Amplifier - Remove the output tube (V6) and clip pin 1 of the output connector to ground. Place the FUNCTION switch on MILLIVOLTS, and turn the ZERO SET and ZERO RANGE controls full clockwise. This puts a large dc error signal across the chopper and input transformer. Use an oscilloscope to check for the presence of 120 cps at the primary of the input transformer (the two outside terminals on the chopper terminal block). Absence of signal means chopper failure (or much less likely, shorted input transformer). Listen for audible chopper action and check chopper drive, if necessary.

If the 120 cps aignal is present, check stage-by-stage throughout the ac amplifier, reducing the input signal as desired by backing off the ZERO RANGE and/or ZERO SET controls, until the failure is discovered.
d. Demodulator Circuit - Check for presence of about 80 volts RMS at the secondary of the demodulator transformer (at the ends of R113 and R114).

The tests outlined above will not suffice to pin-point every fault which may exist. They should, however, lead to the correction of common fallures. In the event that troubles cannot be corrected by these means, or the user finds it more expedient, the unit may be returned to the factory for repair and recalibration at a nominal cost.

## 220 VOLT OPERATION

For 220V operation the power trancfnrmer primary connoctions must be changed. The jumpers connecting black ana black-white together, and blue and blue-white should be removed. The blue lead should be tied to black-white.

| Circuit Des. | Description | Part No. |
| :---: | :---: | :---: |
| Cl01 | Capacitor, mylar selected, 047 to $.33 \mathrm{mfa}, 200 \mathrm{VDCW}$ |  |
| Cl. 0 ? | Capacitor, tubular, olectrolytic, $5 \mathrm{mfd}, 15 \mathrm{VDCW}$ | C12-5 |
| C103 | Capacitor, metalized paper $0.1 \mathrm{mfd}, 200$ VDCW | C18-. 1 |
| C104 | Capacitor, tubular, electrolytic, $20 \mathrm{mfd}, 450$ VDCW | C8-20L |
| Clo'j | Capacitor, mylar dielectric, . 1 mPd , 400 VDCW | C30-. 1 |
| Cl06 | Capacitor, mylar dielectric for 50 cycle model <br> $.0082 \mathrm{mfd}, 1 \%, 100$ VDCW | C45-.0082 |
| Cl07 | Same as Cl02 |  |
| Cl0 | Capacitor, ceramic disc, . $01 \mathrm{mfd}, 600$ VDCW | C22-. 01 |
| C109 | Samo as Cl03 |  |
| Cllo | Seme as ClO4 |  |
| Clll | Same as Cl02 |  |
| Cll2 | Same as Cl05 |  |
| C113 | Capacttor, mylar dielectric, . $333 \mathrm{mfa}, 200 \mathrm{VDCW}$ | C29-. 333 |
| C114 | Capacitor, ceramic disc, . $001 \mathrm{mid}, 600$ VDCW | c22-. 001 |
| C115 | Capacitor, ceramic disc, . 0017 mf , 600 VDCW | C22-:0047 |
| C116 | Same as Cll |  |
| C117 | Capacitor, padding $780-2110 \mathrm{mmf}$ | C51-700-2110 |
| C1.18 | Capacitor, metalized paper, $1.0 \mathrm{mfd}, 200 \mathrm{VDCW}$ | C18-1.0 |
| C501 | Capacitor, tubular, electrolytic, $20 \mathrm{mfd}, 600 \mathrm{VDCW}$ | C35.-20 |
| C502 | Sume as C104 |  |
| C503 | Same as C501 |  |
| C504 | Same as Cl08 |  |
| C50\% | Same as Cl04 |  |
| C506 | Capacitor, mylar dielectric, $4.0 \mathrm{mfd}, 600 \mathrm{VDCW}$ | C50-4.0 |
| C507 | Capacitor, tubular, electrolytic, $1000 \mathrm{mfd}, 12 \mathrm{VDCW}$ | C11-1000 |
| C508 | Same as C507 |  |
| 0509 | Same as C105 |  |
| CHI | Chcke, 200 HY., $120 \mathrm{cps} \mathrm{Hi} Q$ | CHI |
| CSI | Connector, input, special |  |
| CS2 | Connector, output, Amphenol 80 PC 2 F | CS 32 |
| CUl | Chopper, frequency, doubling, special 60 cycle | $\begin{aligned} & \mathrm{Cv2} \\ & \mathrm{Cv} 3 \end{aligned}$ |
| D1 | Diode, Selenium, International Rect. Corp. 501 | RF 15 |
| D2. | Same as Dl |  |
| D3 | Diode, Zener, Hoffman Semiconductor ZAl0 | D2-2A10 |
| D4 | Same as D3 |  |
| F1 | Fuse, $1 \frac{1}{2} \mathrm{~A}, 3 \mathrm{AG}$ (110V), Fuse, $1 \mathrm{~A}, 3 \mathrm{AG}$ (220V) | FU8-FU7 |
| M | Meter, Panel, 200 micro amp zero center | ME-1.4 |
| R101 | Resistor, composition, 33K, $10 \%$, $\frac{1}{2} \mathrm{~N}$ | R1-33K |
| R102 | Resistor, S.S. White, low noise $2 \mathrm{M}, 1 \%$, 1 W | R44-2M |
| $R 103$ | Resistor, cormposition, 47K, 10\%, $\frac{2}{2} \mathrm{~W}$ | R1-47K |
| $\mathrm{R104}$ | Resistor, composition, 1 meg, $10 \%$, $\frac{2}{2} \mathrm{~W}$ | R1-1M |
| R105 | Resistor, composition, 3.3 meg , 1\%, $\frac{1}{2} \mathrm{~W}$ | R1-3.3M |
| R106 | Resistor, deposited carbon, 1 meg, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-1M |
| R10' | Resistor, composition, $22 \mathrm{~K}, 20 \%, \frac{1}{2} \mathrm{~W}$ | Rl-22K |
| R108 | Resistor, composition, $3.3 \mathrm{meg}, 10 \%, \frac{1}{2} \mathrm{~W}$ | R1-3.3M |
| R109 | Same as R1.04 |  |
| R110 | Same as R107 |  |
| R111 | Same as R106 |  |


| Circuit Des. | Description | Part No. |
| :---: | :---: | :---: |
| 81.20 | Resistor, doposited carbon, 200K, if, $\frac{1}{3} \mathrm{~W}$ | K12-200K |
| R113 | Resistor, (ieposited carbon, look, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-100K |
| R114 | Same as R113 |  |
| R11.5 | Resistor, deposited carbon, $1.2 \mathrm{meg} .1 \%, \frac{1}{2} \mathrm{~W}$ | R12-3.214 |
| K110 | Resistor, depositod carbon, 470K, l\%, $\frac{1}{2} \mathrm{~W}$ | R12-470K |
| R117 | Resistor, deposj.ted carbon, 333k, $1 \%$, $\frac{1}{2} \mathrm{~W}$ | R12-333K |
| R118 | Potentiometer 500K ohms | RP5.2 |
| 1219 | Resistor, deposited carbon, 680K, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-0́80í |
| R120 | Sane as RlOj |  |
| R121 | Resistor, deposited carbon, 2.2 meg. $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-2.2M |
| R122 | Resistor, deposited carbon, 6OK, $1{ }_{0}^{\prime \prime}, \frac{1}{2} \mathrm{~W}$ | R12-60K |
| R123 | Same as Rll3 |  |
| R124 | Same as Rlob |  |
| 1225 | Same as R106 |  |
| R126 | Resistor, wlrewound 30K, 10\%, 10W | R5-30K |
| R127 | Potentiometer, J.OK ohms | RP9-10K |
| R12.8 | Resistor, deposited carbon, $96 \mathrm{~K}, 1 \%, \frac{1}{3} \mathrm{~W}$ | R12-96K |
| R129 | Resistor, composition, 22K, 10\%, 2 W | R3-22K |
| R134 | Resistor, special, copper wirewound 10 ohms, low | R18-18-10 |
| K135 | Kesistor, special, copper wirewound loK ohms, 10 | R18-18-10K |
| R136 | Resistor, depositod carbon, special, l. $114,1 \%, \frac{1}{2} W$ | R38-1.11K |
| R137 | Resistor, deposited carbon, special, 100K, 1\%, $\frac{1}{2} \mathrm{~W}$ | R38-100K |
| R138 | Resistor, special, copper wirewound, 10K ohms, $5 \%$ | R18-19.10K |
| R140 | Resistor, deposited carbon, $10 \mathrm{~K}, 1 \%$, $\frac{1}{2} \mathrm{~W}$ | R12-10\% |
| R141 | Rosistor, deposited carbon, 3.33K, $1 \%$, $\frac{1}{2} \mathrm{~W}$ | R12-3.33K |
| R142 | Resistor, deposited carbon, 1K, 1\%, $\frac{1}{2} W$ | R12-1K |
| R143 | Resistor; deposited carbon, 333 ohms, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-333 |
| R1244 | Resistor, deposited carbon, 100 ohms, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-100 |
| R145 | Resistor, deposited carbon, 33.3 ohms, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-33.3 |
| R146 | Resistor, deposited carbon, 10 ohms, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-10 |
| R147 | Resistor, deposited carbon, 3.33 ohms, $1 \%, \frac{1}{2} \mathrm{~W}$ | R12-3.33 |
| 12148 | hesistor, doposited carbon, 1.0 ohms, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-1.0 |
| R149 | Same as Rlob |  |
| R150 | Same as R117 |  |
| R.15. | Same as R113 |  |
| $R 152$ | Resistor, deposited carbon, 33.3K, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-33.3K |
| R153 | Resistor, deposited carbon, 500 ohms, 1\%, 这W | R12-500 |
| 2154 | Same as Rl53 |  |
| R155 | Resistor, deposited carbon, $10 \mathrm{meg}, 1 \%, 1 W$ | R13-10M |
| K156 | Same as R105 . |  |
| R157 | Same as RIO6 |  |
| R158 | Same as R1l7 |  |
| R159 | Resistor, deposited carbon, 99K, $1 \%$, $\frac{1}{2} \mathrm{~W}$ | R12-99K |
| 12160 | Resistor, deposited carbon, 32.3K, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-32.3K |
| R161 | Resistor, deposited carbon, 9K, $10, \frac{1}{2} \mathrm{~W}$ | R12-9K |
| R162 | Resistor, composition, 100K, 10\%, $\frac{1}{2} \mathrm{~W}$ | RI-100K |
| R163 | Resistor, composition, 390K, $10 \%$, $\frac{1}{2} \mathrm{~W}$ | R1-390k |
| R164 | Same as R162 |  |
| R165 | Resistor, composition, $47 \mathrm{~K}, 10 \%, \frac{1}{2} \mathrm{~W}$ | R1-47K |
| 8166 | Resistor, composition, 15K, 10\%, $\frac{1}{2} W$ | R1-15K |
| R167 | Resistor, composition, 4.7K, 10\%, $\frac{1}{2} \mathrm{~W}$ | R1-4.7K |
| R168 | Resistor, composition, $1.5 \mathrm{~K}, 20 \%, \frac{1}{2} \mathrm{~W}$ | R1-1.5K |
| R 169 | Resistor, composition, 4700 ohms, $10 \%, \frac{1}{2} \mathrm{~W}$ | R1-4700 |
| R170 | Resistor, depositod carbon, $1 \mathrm{~K}, 1 \%, \frac{1}{2} \mathrm{~W}$ | R12-1K |


| Circuit Dos. | Description | Part No. |
| :---: | :---: | :---: |
| R1\% 1 | Samo an R106 |  |
| H172 | Same as Rll3 |  |
| R173 | Samo an R16i |  |
| R174 | Potentiometer, 10 turn, 10K | RP4-10K |
| R175 | Resistor, deposited carbon, $100 \mathrm{meg}, 1 \%$, 2 W | R14-100M |
| 1177 | Sano as R127 |  |
| R178 | Resistor, deposited carbon, 75K, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-75k |
| R 179 | Same as R178 - |  |
| R180 | Same as Rl26 |  |
| R 181 | Resistor wirewound, special, customer request only | R18-21-100\% |
| R182 | Resistor, deposited carbon, 1 meg, ly, $\frac{2}{2}$ W customer request | R12-1M |
| R501 | Resistor, composition, 100 ohms, 10,0 , 2 W | R3-100 |
| R502 | Samo as R501 |  |
| R503 | Resistor, wircwound, 5K, 10\%, 10W | RS-5K |
| 8504 | Same as R503 |  |
| R505 | Resistor, composition, 22K, $10 \%$, 2W | R3-22k |
| R506 | Resistor, composition, 10 meg. $10 \%$, $\frac{1}{2} \mathrm{~W}$ | R1-1.0M |
| R507 | Resistor, deposited carbon, 220K ohms, $2 \% \frac{1}{2} W$ | R12-220K |
| 8508 | Same as R101 |  |
| R509 | Same as R101 |  |
| R510 | Same as R106 |  |
| R511 | Resistor, deposited carbon, 600K, 1\%, $\frac{1}{2} \mathrm{~W}$ | R12-600\% |
| R512 | Resistor, wirewound, 6 ohms, $10 \%$, 5W | R4-6 |
| R513 | Resistor, wirewound, 5 ohms, 10\%, 5 W | R4-5 |
| RFI thru RiFlo | Rectifier, selenium, 130v, 65 ma | RF8 |
| RFil | Rectifier, bridge, 26 volt, 600 ma | RF7 |
| SW1 | Function switch, 4 pole, 4 position | SW56 |
| SW2 | Rango switch, 9 position | SW54 |
| SW3 | Zero suppress, zero range 5 position | SW58 |
| SW4 | Power switch, D.P.D.T. | SW14 |
| TRI | Power transformer Central KI-129 | TR27 |
| TR2 | Demodulator transformer Central KI-128 | TR26 |
| TR3 | Input transformer, James $C 1835$ special | TR28 |
|  | Pilot lamps (2) 6.3v. 0.15 anps G.E. type 47 | PL4 |
| V1 | Vacuum tube, type 6084 | EV6084 |
| V2 | Vacuum tube, type EF86 | EV-EF86 |
| V3 | Same as V2 |  |
| V4 | Vacuum tube, type 12AX7 | EV-12AX7 |
| V5 | Vacuum tube, type 12AT7 | EV-12AT7 |
| v6 | Vacuurn tube, type 6cm6 | EV-6CM6 |
| V7 | Vacuum tube, type OA2 | EV-OA2 |
| V8 | Vacuum tube, type 12B1A | EV-12B4A |
| V9 | Vacuum tube, type 5651 | EV-5651 |
| vio | Same as V4 | EV-5651 |

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